



## HAND DELIVERED

January 8, 1996

Mr. Jerry Delevan, P.G. Arkansas Department of Pollution Control and Ecology Water Division P.O. Box 8913 Little Rock, AR 72219-8913

Re: Phase I Groundwater Investigation Report El Dorado Chemical Company WC Project No. 95B165/REPT-1

Dear Mr. Delevan:

Enclosed please find a copy of the summary report for the recent Phase I Groundwater Investigation recently conducted at the El Dorado Chemical Company in El Dorado, Arkansas.

Please contact either of the undersigned at (501)223-2582 with any questions or comments.

Very truly yours, WOODWARD-CLYDE CONSULTANTS

Ray A. Quick, P.G. Office Manager

Encl.

Eric J. Fox Assistant Project Scientist

cc: Mr. John Carver, El Dorado Chemical Company

APR 0 6 1998

# PHASE I

GROUNDWATER

INVESTIGATION

Prepared for El Dorado Chemical Company El Dorado, Arkansas

January 1996

Woodward-Clyde 🗳

Three Financial Centre 900 S. Shackleford, Suite 412 Little Rock, AR 72211

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#### 1.0 INTRODUCTION

In compliance with the terms of Paragraph 18 of Consent Administrative Order (CAO) LIS 95-070, El Dorado Chemical Company (EDC) submits this report summarizing the results of a concentrated Phase I Groundwater Investigation. The Phase I investigation was conducted in accordance with a Groundwater Monitoring Work Plan (GMWP) dated September 19, 1995, and approved by the Water Division of the Arkansas Department of Pollution Control and Ecology (ADPC&E) on October 12, 1995.

This Phase I investigation addressed the following areas of potential concern (APCs) at the EDC facility:

- Process Wastewater Treatment System (PWTS), including:
  - 1. Lake Lee
  - 2. Lake Kildeer
  - 3. Plant Drain System
- Nitric Acid Concentrator Area
- Product Loading and Unloading Areas

As stated in the CAO, these areas are suspected to be potential sources of release for one or more of the following parameters:

- Nitrate
- Sulfate
- Lead
- Chromium

As proposed in the approved GMWP, definition of the groundwater quality beneath the EDC site is being conducted through a phased approach. Phase I consisted of the preliminary delineation of shallow groundwater quality at 35 locations throughout the facility using direct-push technology and groundwater sampling and analysis. A proposed scope of work for the second phase of investigation has been developed based on the Phase I results and is provided in Section 6.0 of this report.

This report has been divided into the following sections:

- Section 2.0 provides a summary of the site environmental setting and the results of relevant previous environmental investigations conducted at the EDC facility
- Section 3.0 details the methodologies employed in the Phase I groundwater investigation, including the installation and sampling of temporary well points at 35 locations throughout the EDC facility
- Section 4.0 provides a summary of the preliminary groundwater elevation and quality data obtained during this initial phase of investigation
- Section 5.0 presents the conclusions based on the Phase I data
- Section 6.0 provides the recommendations for additional investigation, including a proposed scope of work for a Phase II groundwater investigation involving installation of a network of groundwater monitoring wells
- Section 7.0 details a schedule for implementation of the proposed Phase II groundwater investigation.

## 2.1 FACILITY LOCATION

The EDC facility is located at 4500 North West Avenue in the city of El Dorado, Union County, Arkansas. The EDC property consists of approximately 1,340 acres, of which about 150 acres are utilized for plant operations (i.e., production and support areas). The approximate center of the Production Area is located at Latitude 33° 15′ 53″ North, Longitude 94° 41′ 16″ West and is generally contained in the southeast 1/4 of Section 6 and the northeast 1/4 of Section 7, Township 17 South, Range 15 West. A site location plan of the EDC facility is presented in Figure 1.

## 2.2 FACILITY DESCRIPTION AND HISTORY

EDC is a manufacturer of basic agricultural chemicals, including sulfuric acid, nitric acid, ammonium nitrate fertilizers and industrial grade ammonium nitrate. Ammonia used in the manufacture of nitric acid and ammonium nitrate is received at the plant site through an underground pipeline owned and operated by Lone Star Industries. Elemental sulfur used in the manufacture of sulfuric acid is received via rail car shipment. The other principal raw materials used in the production processes at EDC are water and natural gas. Water is supplied through five on-site operating production wells, owned by EDC and ranging in depth from 530 feet to 670 feet below ground surface. Natural gas is supplied to the plant through an underground pipeline owned and operated by Arkansas-Louisiana Gas Company.

The EDC facility is currently owned by El Dorado Chemical Company, a wholly owned subsidiary of LSB Industries of Oklahoma City, Oklahoma. EDC purchased the plant in July, 1983 from Monsanto Chemical Company, which had occupied the site since 1955. Previous site occupants included the Lion Oil Company (1949-1955) and the Lion Chemical Corporation (1943-1949). Based on information provided by EDC, the plant property was undeveloped prior to 1943. Since 1943, site operations have generally been limited to production of ammonia-related products and sulfuric acid.

## 2.3 REGIONAL GEOLOGIC AND HYDROGEOLOGIC SETTING

The EDC facility lies within the Gulf Coastal Plain Province in southern Arkansas. Heath (1988) has broadly characterized this province as a relatively undissected low-lying plain underlain by complexly interbedded sands, silts, and clays which thicken progressively

toward the coast and toward the Mississippi River. Sediments within the sequence are, for the most part, unconsolidated or non-lithified. The sediments range in age from Quaternary (youngest) to Triassic. The sediments occur as continuous, distinguishable units across most of the Gulf Coastal Plain Province.

Structurally, depositional dip was basinward in a generally southern to southeasterly direction. Growth fault development at depth enhances the basinward dip of the sediment accumulations across the region. A graben structure (a down-thrown faulted block of sediments) is located approximately seven miles south of the facility. The fault planes which form the graben strike northwest-southeast.

Table 1 shows the age relationships of the various formations found in the subsurface of the region. Also shown are the approximate thickness of each formations and descriptions of the hydrogeologic character of the sediments.

Broom, et. al. (1984) have characterized the regional hydrogeology in a study of salt water contamination of groundwater in Union County, Arkansas. The regional hydrogeologic description presented here is based largely on their work. Additionally, two studies (Fitzpatrick, et. al., 1990 and McWreath, et. al., 1991) which simulated the response to pumping stresses in the Sparta aquifer are also cited in description of the regional hydrogeologic setting. The major regional aquifers and confining units of the region are presented in Figure 2. The following discussions are limited to the principal aquifers used for potable water supplies within the immediate vicinity of the EDC site: the Cockfield aquifer, the Greensand aquifer, and the El Dorado aquifer. The Greensand aquifer and the El Dorado aquifer.

## 2.3.1 Cockfield Aquifer

The Tertiary-aged Cockfield Formation (part of the Claiborne Group) crops out over most of Union County. This formation consists predominantly of sands, silts, and carbonaceous (calcitic) clays with minor amounts of interbedded lignite and gypsum. The formation can contain lenticular beds of lignitic sands in some areas. The formation thickness is approximately 200 feet in most of the county. A thin veneer of Quaternary-aged alluvial sediments overlay the Cockfield Formation along the Ouachita River and its tributaries.

Recharge to the Cockfield aquifer is local. Groundwater occurs under water table, or unconfined, conditions; however, locally semi-confined conditions have been demonstrated to exist in areas where the clay content of the overlying sediments is high. Water table configuration within the aquifer generally exhibits a subdued reflection of the local topography with flow toward surface drainages (i.e., the valleys of the principal streams). Water levels in wells range in depth from near land surface in low-lying areas to as much as 50 feet deep on the tallest hills and ridges.

Falling head tests on undisturbed samples collected from the Cockfield Formation revealed coefficient of vertical permeability values ranging from  $1.0 \times 10^{-3}$  cm/sec for sandy materials to  $5.0 \times 10^{-8}$  cm/sec for the more clayey sediments. This wide range of permeability values is the result of the variable lithologic character of the sediments. Lithologic investigations have shown that the Cockfield Formation is highly variable in clay content with some areas being predominantly clay and other areas being predominantly sand. The horizontal hydraulic conductivity of the aquifer, when considered as a whole, is generally greater than the aquifer's vertical hydraulic conductivity. Areas of high clay content tend to perch groundwater on a local scale. Further, clay horizons can generate semi-confined conditions when the clayey material overlies more permeable zones and hydrostatic head is driven by recharge areas at higher elevations.

Domestic use of groundwater from the Cockfield aquifer has decreased considerably in recent years. Prior to the 1920s, the Cockfield aquifer was the primary source of groundwater for both domestic and industrial use. Rural water supply systems developed in the late 1960s greatly reduced the number of wells producing from the Cockfield aquifer (Broom, et. al., 1984).

## 2.3.2 Cook Mountain Formation

The Cook Mountain Formation underlies the Cockfield Formation in all areas of the region except where the younger Cockfield sediments have been removed by erosion and the Cook Mountain Formation is exposed at the surface. The Cook Mountain Formation consists of low permeability clays and silty clays with lesser amounts of very fine sands. The formation acts as a lower confining unit (aquitard) for the Cockfield aquifer and an upper confining unit for the underlying Sparta aquifer.

Green ...

Thickness of the confining unit is variable, ranging from approximately 50 feet to 200 feet across the region. Based on Woodward-Clyde's review of boring logs for area production wells, the thickness of the confining unit is estimated at approximately 200 feet in the vicinity of the EDC facility.

Vertical hydraulic conductivity of the confining unit was estimated by Fitzpatrick, et. al. (1990) to range from  $1 \ge 10^{-7}$  cm/sec to  $1 \ge 10^{-10}$  cm/sec. The estimates are based on the results of their calibrated regional finite-difference model. Horizontal hydraulic conductivity

of the Cook Mountain confining unit was established by the calibrated model to be  $3.18 \times 10^{-9}$  cm/sec. Therefore, both the vertical and horizontal hydrologic flow components are retarded by this formation.

## 2.3.3 Sparta Formation

The Tertiary-aged Sparta Formation is the main source of municipal and industrial water supplies throughout the region. Heavy pumping stresses placed on the aquifer in the past decades have created large cones of depression within the potentiometric surface surrounding the pumping centers. One such cone of depression is centered around the city of El Dorado. Large quantities of groundwater withdrawn from the aquifer have altered, and in some cases reversed, flow directions in the aquifer (McWreath, et. al., 1991).

In Union County, the Sparta Formation is hydrostratigraphically separated into three zones based on lithologic character and water production capacities. These zones, in descending order, are the Greensand aquifer, the Sparta Formation confining bed, and the El Dorado aquifer. The El Dorado aquifer is the most heavily used portion of this hydrostratigraphic sequence.

## 2.3.3.1 Greensand Aquifer

The Greensand aquifer occupies the upper portion of the Sparta Formation. The aquifer consists of fine-grained to very fine-grained glauconitic sands with lesser amounts of silts and clays. Groundwater within the aquifer is under confined conditions. The Greensand aquifer is located below the Cook Mountain confining unit, and above a clay-rich horizon of the Sparta Sand which acts as a lower confining unit.

The structural top of the aquifer in the vicinity of El Dorado ranges from mean sea level (msl) to 50 feet below msl, yet the potentiometric surface in tightly cased wells can rise as high as 100 feet above msl in some areas. The Greensand aquifer thickness in the Union County area is approximately 200 feet (Leidy and Taylor, 1992). The regional flow direction within the aquifer is south-southeast (Broom, et. al., 1984).

The Greensand aquifer is used as a potable water supply, but less extensively than the deeper, more productive El Dorado aquifer. Recharge to the Greensand aquifer is via precipitation and from streams flowing across outcrop areas. To a lesser extent, the aquifer can receive recharge from leakage across confining beds when the vertical hydraulic gradient is toward the aquifer.

#### 2.3.3.2 Sparta Sand Confining Bed

In separate investigations by Fitzpatrick, et. al (1990) and McWreath, et. al. (1991), the Sparta Formation has been treated as a single aquifer for the purposes of finite-difference modeling of the effects of pumping stresses. However, as stated by Broom, et. al. (1984), sufficient evidence exists to support the conceptualization that in Union County, Arkansas a predominantly marine clay horizon in the middle portion of the Sparta Formation serves as a confining unit. Hydraulic conductivity, both horizontal and vertical, is low in comparison to the overlying and underlying sediments. This zone serves as a confining bed between the upper and lower portions of the Sparta Formation and allows them to function separately as individual aquifers. McWreath, Nelson, and Fitzpatrick (1991) support the designation of this clay horizon as a confining unit on a local scale. The confining bed is between 50 and 150 feet thick in the Union County area (McWreath, et. al., 1991).

#### 2.3.3.3 El Dorado Aquifer

The El Dorado aquifer is more productive and, thus, more heavily targeted for placement of high yield wells. The City of El Dorado and local industries have production and/or supply wells completed in this aquifer.

The structural top of the aquifer in the vicinity of the EDC facility is estimated to be approximately 350 feet below msl. Thickness of the aquifer in this area is approximately 200 feet (Broom, et. al., 1984).

## 2.4 PREVIOUS ON-SITE INVESTIGATIONS

Five previous hydrogeologic investigations have been completed which have focused on shallow groundwater conditions at four locations at the EDC facility. Generally, these investigations confirm the information regarding shallow groundwater as given in the preceding discussion of regional geologic and hydrogeologic settings. The investigations are summarized below.

#### 2.4.1 McClelland Engineers - 1980 Investigation

McClelland Engineers completed an investigation in the west-central portion of the EDC property in December, 1980 (McClelland Engineers, 1980). The stated investigation objectives were to:

- Determine general soil stratigraphy at the site in relation to groundwater characteristics
- Establish the thickness and character of the existing soil strata
- Establish the permeability of significant strata
- Install wells for long-term monitoring of groundwater quality

The study concluded that the west-central portion of the site was underlain by deposits of the Claiborne Group. At the site, the "upper approximately 10 to 15 feet consists of reworked alluvial deposits; whereas the underlying beds are relatively unaltered from the original depositional character." Cover soil in the area was found to range from 2 to 2.5 feet in thickness in four borings. The cover soil was reported to consist predominantly of gray and tan sandy clay with the percentage of sand varying from 6 to 37 percent.

At the site, "moderately variable stratigraphy and cross-bedding should be anticipated." In four widely spaced borings around the area of the site currently occupied by the Class III landfill, McClelland noted significant variation in strata. The borings for monitoring well installations were advanced by a combination of dry auger and wash-rotary drilling methods and were completed to depths ranging from 20 to 40 feet. The Plan of Borings (Plate 1 of the McClelland report) indicates that four borings, (i.e., B-A, B-B, B-C and B-D) were completed as groundwater monitoring wells. However, the text indicates that two additional borings, C-1 and C-2, were completed in the vicinity of boring B-C, although borings logs were not provided for these locations. In addition, there are no monitoring well installation diagrams or other information to indicate at what depth well screens have been placed at these wells.

Groundwater was reportedly encountered in the borings at depths ranging from 7.5 to 21 feet below grade. In each boring, the water level was observed to rise rapidly. The recorded amount of rise ranged from 3.5 feet in Boring C-2 (completed to 10 feet total depth) to 16.5 feet in Boring B-C (completed to 40 feet total depth). McClelland interpreted the water level information to represent, "a 'perched' condition rather than a major groundwater aquifer."

The water levels in B-C (completed at 40 feet total depth) and C-2 (completed at 10 feet total depth) both rose to 4.5 feet below grade. However, the water level in Boring C-1 (completed to 20 feet total depth) rose only to 14 feet below grade. McClelland reported vertical permeability values for the cover in the area ranging from  $1.0 \times 10^{-6}$  to  $1.0 \times 10^{-7}$  cm/sec. The vertical permeability of the natural clays which are assumed to underlie the cover are reported to range from  $5.0 \text{ to } 10^{-7}$  to  $1.0 \text{ to } 10^{-8}$  cm/sec.

Woodward-Clyde infers from the McClelland report and general geologic conditions of the region that the clay layers may not be continuous across the entire area; the overall vertical permeability value for the area as a whole should not exceed approximately  $1 \times 10^{-7}$  to  $5 \times 10^{-7}$  cm/sec. In areas where sand interbedding is prevalent, the overall horizontal permeability value may locally approach  $1.0 \times 10^{-5}$  to  $1.0 \times 10^{-4}$  cm/sec.

#### 2.4.2 McClelland Engineers - 1981(a) Investigation

McClelland Engineers completed an investigation in the Lake Kildeer Area in June, 1981 (1981(a)). The studies were conducted to provide the following:

- General subsurface stratigraphy and definition of the first aquifer
- Determination of the degree of contamination, if any, of the first aquifer and soils resulting from seepage losses from the impoundment
- An estimation of the seepage losses based on groundwater seepage analysis and a water balance for existing and proposed reservoir levels

The study concluded that the site was underlain by deposits of the Claiborne Group. A total of 12 borings were completed with depths ranging from 18 to 100 feet below grade using a combination of dry auger and wash-rotary methods. Casagrande-type piezometers were installed in six of the borings (Borings A through F). These were reported to consist of 2-inch diameter closed-end PVC casing with a slotted screen tip approximately 3 to 4 feet in length. The annulus around the well screen was backfilled with a graded, free-draining sand. A layer of bentonite pellets was placed above the sand pack, and the annulus was sealed with grout to prevent infiltration of surface water.

Six monitoring wells were also installed, at Borings 1, 2, 2A, 3, 4 and 5. The monitoring wells were reportedly installed in a similar manner as the Casagrande piezometers. However, the wells incorporated 4-inch diameter casings, 5-foot slotted screen lengths and 2-foot sand traps. A plan of the borings, boring location coordinates, boring ground surface elevations and Boring Logs are presented in the McClelland report. Information on screen placement is indicated on the Boring Logs. According to the Plan of Borings:

- Piezometer F and Monitoring Well 1 (MW-1) were completed in a former borrow area located adjacent to the north end of the lake
- Piezometer A was completed near the northeast corner of the lake
- Piezometer E was completed north of the northern end of the dam
- Piezometer D and MW-2, MW-2A, and MW-5 were completed east and downstream of the dam

- Piezometer C was completed south of the southern end of the dam
- MW-3 was completed east of the accessory dike on the southern side of the lake
- MW-4 was completed near the end of the western end of the accessory dike on the southern side of the lake
- Piezometer B was completed near the western end of the accessory dike on the southern side of the lake

McClelland divided the deposits encountered in these borings into three strata as follows:

"STRATUM I: Stiff to very stiff tan and gray sandy clay (CL) was encountered at or near the ground surface over a portion of the site to depths of up to approximately 15 ft. The permeability of this stratum is estimated to be in the order of  $1.0 \times 10^{-7}$ centimeters per second.

STRATUM II: Medium dense to dense gray clayey sand and silty sand (SC and SM) was encountered beneath Stratum I or at the ground surface over most of the site to depths of up to approximately 50 ft. The thickness of this stratum is greatest on the south side of the Impoundment Pond and beneath the embankment (approximately 30 to 50 ft.) and least on the north and west sides of the pond (approximately 0 to 20 ft). Measured permeability values were found to vary widely over the range of  $1.3 \times 10^{-4}$  to  $5.8 \times 10^{-7}$  centimeters per second.

STRATUM III: Laminated stiff to very stiff gray silty clay (CL and CH) and light gray fine sand (SM was encountered as the basal unit beneath Strata I and II). This stratum was encountered generally below EL 160 to 170 on the northwest sides of the impoundment, below EL 130 on the south side and below EL 90 to 100 in the valley bottom below the dam. Measured permeabilities range from  $9.5 \times 10^{-5}$  to  $7.0 \times 10^{-9}$  centimeters per second. Vertical permeabilities are substantially less than horizontal permeabilities in this laminated zone."

It is not clear from the report whether the strata described above should be treated as one or more water bearing zones. The wells and piezometers have their screens set in Stratum II (MW-1, MW-3, MW-4 and MW-5 and Piezometers B, C and D) and in Stratum III (MW-2 and Piezometers A, E and F). MW-2A is apparently screened in shallow fill material. McClelland concluded that regional groundwater flow in the uppermost aquifer was from the north-northwest to the south-southeast. Based on chemical analytical data from the investigation, McClelland concluded that "little if any contamination of either the soil or groundwater was evidenced in the chemical analyses."

Based on seepage analyses and a water balance, McClelland estimated that underseepage losses from Lake Kildeer range from 300 gallons per day (gpd) with a lake surface elevation of 165 feet above mean sea level (msl) to 700 gpd with a lake water surface elevation of 175 feet above msl. Details of the seepage loss estimates are not provided in the report but it is noted that, "considerably higher or lower seepage quantities could actually be experienced."

## 2.4.3 McClelland Engineers - 1981(b) Investigation

McClelland Engineers completed an investigation of the Lake Lee area in November, 1981 (1981(b)) to address potential contamination of the "uppermost aquifer" due to construction of the collection pond. Four borings were completed to depths ranging from 40 to 60 feet using a combination of dry auger and wash-rotary methods. The boring locations were selected to provide three downgradient (Borings 1, 2 and 3) and one upgradient (Boring 4) locations. The report does not indicate that monitoring wells were installed. Monsanto Company representatives collected water samples immediately on the first encounter of water in each boring. These water samples were tested for pH, sulfate, nitrate-nitrogen and ammonia-nitrogen. A variable head aquifer test was also performed on Boring 3.

The report concluded that Lake Lee was underlain at depth by deposits of the Claiborne Group. These were encountered at elevations below 162 to 164 feet above msl within the pond area and below 147 feet above msl downgradient of the pond. Fill or alluvium was encountered above the Claiborne deposits. McClelland divided the deposits encountered in these borings into four strata as follows:

"Stratum I: Fill consisting of very stiff to firm tan gray and brown sandy clay (CL) with some gravel encountered at the ground surface to depths of 5 to 17 feet (generally to EL 166 to 170 within the pond area). The mass permeability of this stratum is in the order of  $7 \times 10^{-7}$  to  $5 \times 10^{-8}$  cm/sec.

Stratum II: Soft to stiff gray with tan sandy clay (CL) was encountered beneath the fill to depths of approximately 15 to 20 ft. This stratum contains some silty sand pockets and seams and consequently possesses a horizontal permeability in the order of  $5.0 \times 10^{-6}$  to  $1 \times 10^{-5}$  cm/sec. This stratum represents geologically recent alluvial deposition.

Stratum III: Very stiff brown and dark gray clay (CL to CH) with light gray silt and fine sand partings and seams was encountered beneath the alluvial zone to the completion depths of 40 ft. in Borings 1, 2 and 4 and to a depth of 49 ft. in Boring 3.

Numerous sand seams and layers were encountered below depths of 35 ft. in Boring 3 and 32.5 ft. in Boring 4. The mass vertical permeability of this stratum is in the order of 5 x  $10^{-8}$  to 1 x  $10^{-7}$  cm/sec. In the deeper zone more frequent sand seams are encountered and the mass vertical permeability could approach 1 x  $10^{-5}$  and 1 x  $10^{-4}$  cm/sec.

Stratum IV: Dense light find sand (SN to SP) with occasional clayey seams was encountered beneath Stratum III in Boring 3 at a depth of 49 ft. The coefficient of permeability is estimated to be  $1.0 \times 10^{-3}$  cm per second for this sand stratum."

Static groundwater levels in the four borings ranged from 4 feet below grade in Boring 3 to 24.5 feet below grade in Boring 1. The groundwater flow direction roughly paralleled the ground surface and sloped downward towards the southeast. McClelland concluded that the water bearing zone encountered did not represent the uppermost aquifer. The uppermost aquifer was interpreted as being in the Stratum IV sands encountered below 115 msl.

## 2.4.4 MCI Consulting Engineers - 1985 Investigation

A second investigation was completed in the Lake Lee area in 1985 by MCI Consulting Engineers, Inc. (MCI). This investigation was undertaken in support of EDC's RCRA Part B Permit Application, which was subsequently withdrawn. A formal report of this second Lake Lee investigation was not prepared, although it was summarized and referenced in the Groundwater Protection section of the Part B Permit Application (EDC, 1986).

The investigation involved installation of four borings and piezometers around Lake Lee, identified as L-1 through L-4. Well installation diagrams indicate that each monitoring well was constructed of 2-inch diameter threaded PVC riser pipe and five feet of 0.010-inch slot PVC well screen. Downgradient wells L-2, L-3 and L-4 were installed to a depth of 20 feet, while upgradient well L-1 was installed to 25 feet. The annular space between the screen and soil is backfilled with sand, and a bentonite pellet seal was placed above the sand pack. The remainder of the boring was grouted with bentonite/cement grout. A potentiometric map which accompanies the logs and well installation diagrams indicates the groundwater flow direction is towards the northeast, which contradicts the information presented in the McClelland (1981b) report.

#### 2.4.5 Grubbs, Garner & Hoskyn - 1992 Investigation

Grubbs, Garner & Hoskyn (GGH)(1992) completed an investigation of the existing Class III Landfill in September, 1992. The objectives of this study were to define site stratigraphy,

and to determine groundwater depth and movement. Three borings were completed to depths ranging from 20 to 25 feet below grade using dry auger methods. Monitoring wells were installed in each of the three borings. Monitoring wells were constructed of 2-inch diameter PVC risers and 0.010-inch slot PVC well screen. The annulus between the screen and soil was backfilled with a 10/20 sand pack, and a bentonite pellet seal was placed on top of the sand pack. The remaining annular space was then filled to near the ground surface with cement/bentonite grout. Well completion details are shown on the boring logs provided in the report.

EDC personnel have stated that the GGH Report has the designations for Monitoring Well 1 and Monitoring Well 3 reversed from EDC's understanding of the monitoring well designations. Therefore, this section of this report follows the monitoring well designation understood by EDC (i.e., Monitoring Well 1 is located east of Landfill Area 1 and Monitoring Well 3 is located south of Landfill Area 5). For excerpts of the report that are in direct quotes, Woodward-Clyde will recite the GGH report as written, but will insert the EDC designations in parentheses.

The Class III Landfill site was found to be underlain by deposits of the Claiborne Group. Based on available mapping, GGH projected that the base of the Cockfield and the top of the Cook Mountain Formation will be encountered at a depth of about 100 feet below grade at the site. GGH estimated the thickness of the Cook Mountain clays at approximately 150 to 200 feet at the EDC site.

GGH summarized the stratigraphy encountered in borings at the site as follows:

"Stratum I: Loose to medium-dense brown, tan and gray clayey silt and silty fine sand to fine sandy silt was encountered at the ground surface to depths of 2 to 4 ft.

Stratum II: Stiff to very stiff gray and yellowish tan clay and sandy clay with silty sand seams was encountered beneath Stratum I to depths of 13 to 20 ft. The more clayey portions of this stratum were found to possess vertical hydraulic conductivities in the range of  $3 \times 10^{-9}$  to  $5 \times 10^{-9}$  cm/sec. Due to the presence of intermittent sand seams, horizontal hydraulic conductivities are substantially greater than these recorded vertical conductivities.

Stratum III: Medium dense to dense tan and gray silty fine sand was encountered beneath Stratum II in Monitoring Wells 2 and 3 (EDC Well 1) to the boring completion depths. Grain size analyses indicated hydraulic conductivities ranging from 4 x 10<sup>-4</sup> to 8 x 10<sup>-4</sup> cm/sec. Review of this and previous studies indicates that this sand stratum is present over most of the existing and old landfill sites.

Stratum IV: Very stiff, dark brown clay was encountered beneath Stratum III in Monitoring Well 1 (EDC Well 3) to the boring completion depth. A coefficient of permeability of  $5 \times 10^{-9}$  cm/sec was obtained. This clay stratum was also encountered in Boring 3 of the previous study. Apparently, this predominantly clay unit is confined to the northeastern portion of the existing landfill."

GGH provided a potentiometric surface map using groundwater elevation data obtained from the three recently installed wells at the existing landfill and groundwater elevation data from the four older wells installed at the old Monsanto Landfill. However, GGH noted that the groundwater elevations in Wells B-A and B-C-2 at the old landfill were considered to represent "perched" conditions in association with near surface sand units at those wells. Thus, groundwater surface elevations from these two wells were excluded in the preparation of the GGH potentiometric surface map.

The potentiometric surface map prepared by GGH indicates that shallow groundwater flow is generally to the southeast beneath the Monsanto Landfill and generally to the south beneath the existing Class III Landfill. Woodward-Clyde notes that this flow direction is toward the valley of the unnamed tributary that crosses the EDC property on the south side of the Production Area.

## 2.5 AREAS OF POTENTIAL CONCERN

In September, 1992, the Superfund Branch of the Hazardous Waste Division of the ADPC&E conducted a preliminary assessment of the environmental conditions at the EDC facility. The investigation was completed under the authority of the federal Comprehensive Environmental Response, Compensation and Liability Act (CERCLA) and the Superfund Amendments Reauthorization Act (SARA) with the overall objective of determining if additional CERCLA/SARA actions at the facility are warranted.

An on-site and off-site reconnaissance were completed by the ADPC&E on September 9-10, 1992. A report of the preliminary assessment was issued by the ADPC&E on September 30, 1992 and later revised on October 27, 1992. Based on the findings of the preliminary assessment, the ADPC&E identified the plant's wastewater treatment system and Lake Lee as areas of potential concern (APCs).

In March of 1994, a multi-media inspection (MMI) of the EDC facility was conducted by the ADPC&E. As part of the MMI, personnel from the Water Division of the ADPC&E conducted an inspection of the process wastewater treatment system, and the EDC facility in general. The inspection included a groundwater monitoring data review which revealed that nitrate in groundwater had been detected at concentrations in excess of the United States Environmental Protection Agency's (USEPA's) Maximum Contaminant Level (MCL) for nitrate (10 mg/L, EPA 1993). In addition, sulfate had been detected at concentrations above the USEPA's secondary MCL (SMCL) for sulfate (250 mg/L, EPA 1993).

On March 29, 1994, Water Division personnel reported the findings of the inspection and recommendations for actions to be taken by EDC. This information was detailed in a memorandum to the enforcement coordinator (Mr. Harry Elliott) of the MMI task force.

Based on the findings of the September, 1992 preliminary assessment and the March 1994 MMI, a Consent Administrative Order (CAO) was negotiated between EDC and the ADPC&E and became effective on June 6, 1995. Paragraph 18 of the CAO specifically cited the following areas to be of potential concern with respect to groundwater quality:

- Process Wastewater Treatment System (PWTS), including:
  - 1. Lake Lee
  - 2. Lake Kildeer
  - 3. Plant Drainage System
- Nitric Acid Concentrator Area
- Product Loading and Unloading areas

Figure 3 presents the locations of these APCs, as well as each of the temporary well point locations.

The APCs addressed in the CAO are suspected to be potential sources of release for nitrate and sulfate. Lead and chromium were also identified as targeted parameters in the CAO due to the inadvertent disposal of a sludge containing lead and chromium in EDC's Class III Landfill. The four targeted parameters for the Phase I and Phase II Groundwater Investigation are summarized below:

<u>Nitrate</u>: Process wastewater from the nitric acid manufacturing process is likely to contain a significant concentration of nitrogen-related compounds, including nitrate. Nitrate does not typically occur in natural waters at significant concentrations, and its presence would indicate likely wastewater

contamination and/or a lack of oxidizing conditions. The current USEPA MCL for nitrate is 10 mg/L.

Sulfate: Process wastewater from the sulfuric acid manufacturing process is likely to contain a significant concentration of sulfates. Although sulfate occurs in almost all natural water at low concentrations, its presence at high concentrations may pose a human health hazard. The current proposed USEPA MCL for sulfate is 500 mg/L (USEPA, May 1995).

## Lead and

Chromium: In accordance with permit 0177-SR-1, solid sulfur sludge from the facility's nitric acid concentrator tanks was periodically disposed of in the Solid Sulfur Disposal Cell (SSDC) of EDC's Class III Landfill. In May 1993, impacted sludge characterized by a blue-green appearance was observed during disposal operations. The sludge was removed and placed into drums for characterization, whereby elevated levels of leachable lead and chromium were quantified in grab samples. EDC attributed the elevated levels of lead and chromium to corrosion of the Lewmet dip tube and certain lead lined components of the nitric acid concentrator unit. Approximately 218 tons of sludge and soil were excavated, removed, and transported off-site to a RCRA-permitted hazardous waste landfill. From August through October 1995, waste material remaining in the SSDC was stabilized and covered with a low permeability clay cap, and the Class III landfill was closed in accordance with EDC's approved Consolidated Plan for Closure of the Class III Solid Waste Landfill and Corrective Action Plan for the Solid Sulfur Disposal Cell (June 1995). The current state regulatory action level for lead in groundwater is 0.015 mg/L, while the USEPA MCL for chromium is 0.1 mg/L.

The following discussion gives a brief overview and description of the areas of potential concern (APCs) identified in the CAO.

#### 2.5.1 Process Wastewater Treatment System (PWTS)

The PWTS receives flows from the following equipment within the EDC facility's production area:

- Three weak nitric acid plants
- Two ammonium nitrate plants
- One sulfuric acid plant

- One natural gas fired boiler
- One nitric acid concentrator
- One strong nitric acid plant with associated oxygen plant

Process wastewater from these areas is subsequently discharged to three associated APCs, namely Lake Lee, Lake Kildeer, and the plant drainage system.

## 2.5.1.1 Lake Lee

Lake Lee is a one-acre pond equipped with an aerator. Under high rainfall conditions, wastewater mixed with stormwater from the acid manufacturing area can bypass the neutralization pit and flow directly to Lake Lee. Lake Lee also receives direct flow from the ammonium nitrate plants, boiler blowdown, and zeolite regeneration backwash. These three sources are mixed by the aerator in Lake Lee. From Lake Lee, flow is directed through a pipe to Lake Kildeer in the south-central portion of the EDC property.

Under normal conditions, all stormwater flows are treated with the process wastewater. However, when stormwater volumes exceed the capacity of the pipe from Lake Lee to Lake Kildeer, the excess flow is directed through an overflow pipe from Lake Lee and is discharged through Outfall 002 into the tributary of Haynes Creek. This overflow pipe is necessary for levee protection for Lake Lee.

## 2.5.1.2 Lake Kildeer

Lake Kildeer is a fifty-acre  $(\pm)$  finishing treatment pond which allows retention time for biological treatment. Discharge from Lake Kildeer is via Outfall 001 to an unnamed tributary of Haynes Creek.

#### 2.5.1.3 Plant Drainage System

The plant drainage system is comprised of four components:

- Discharges from the PWTS through NPDES Outfall 001
- Discharges of stormwater/wastewater under heavy rainfall conditions through NPDES Outfall 002
- Discharges of effluent from the sanitary sewer collection and treatment system through NPDES Outfall 003
- Discharges of stormwater collected around the ammonium nitrate manufacturing and loading/unloading areas through NPDES Outfall 004

A schematic showing the arrangement of the plant drainage and discharge (including the PWTS) is presented in Figure 4. Figure 4 also shows the location of the sanitary sewer treatment system and the NPDES regulated stormwater discharge outfalls.

NPDES Outfall 001 discharges the processed wastewater and stormwater from EDC's acid manufacturing and ammonium nitrate manufacturing operations. Inlets to the system receive flows released continuously from cooling towers, boiler blowdowns, and manufacturing areas where there is potential for spills (both indoor and outdoor). Flows enter the process sewer system and flow by gravity to a pumping station located on the south side of the acid manufacturing area. At this point, the wastewater is pumped from a stainless steel collection basin and into a limestone (CaCO<sub>3</sub>) neutralization basin. Flow from the neutralization basin is via gravity into Lake Lee, which is also referred to as the day pond.

Sanitary wastewater is collected and treated by a separate system at the EDC facility. The wastewater is collected and transferred via gravity flow to an Imhoff sanitary treatment plant located approximately ¼ mile south of the manufacturing area. After treatment, effluent is discharged to the unnamed tributary of Haynes Creek at a location downstream of the other outfalls.

## 2.5.2 Nitric Acid Concentrator Area

Within the EDC facility's production area, flow from one nitric acid concentrator, three weak nitric acid plants, and one strong nitric acid plant with associated oxygen plant is directed to the PWTS. Flow from cooling towers, boiler blowdowns, and manufacturing areas enter the process sewer system and flow by gravity to a pumping station located on the south side of the acid manufacturing area. The wastewater is then pumped from the stainless steel collection basin and into a limestone (CaCO<sub>3</sub>) neutralization basin prior to gravity discharge to Lake Lee.

## 2.5.3 Product Loading and Unloading Areas

Stormwater which falls in the vicinity of the ammonium nitrate manufacturing area and the product loading/unloading areas is collected in storm sewers and is directed to an 18" diameter polyethylene sewer pipe which carries the flow along the western and southern sides of the production area. Discharge from this pipe is directly to Lake Lee, where the water is aerated prior to discharge to Lake Kildeer. When runoff exceeds the capacity of this system, overflow is directed through Outfall 004 and into the unnamed tributary of Haynes Creek.

#### 3.0 METHODS OF INVESTIGATION

## 3.1 WELL POINT PROGRAM

The ADPC&E-approved Groundwater Monitoring Work Plan outlined a phased approach for investigating groundwater quality beneath various portions of the EDC site. The first phase of investigation utilized a Hydropunch direct-push sampling device to install temporary well points at thirty-five (35) locations around the EDC site. The principal objectives of the well point program were to obtain preliminary groundwater elevation and quality data from a number of locations around each APC in order to provide a broad indication of the groundwater flow direction and groundwater quality. This data was then utilized for the preparation of Phase II recommendations which are outlined in Section 6.0.

#### 3.1.1 Well Point Installation

The temporary well points were installed by GEO Environmental, Inc. (GEO) using a Hydropunch sampling system, which consists of a direct-push sampling device mounted on a pickup truck. The work was done under the observation of Woodward-Clyde field personnel.

Well point installation was accomplished by attaching an expendable well point to the leading end of a series of one-inch outer diameter stainless steel probe rods, which were hydraulically driven into the ground to the desired depth. The well point was attached to the probe rod using clean, laboratory-grade film to avoid down-hole contamination. Upon achieving the desired depth, perforated 3/8" polyethylene tubing was placed down the inner circumference of the probe rods, and threaded into the expendable well point. With the well point acting as an anchor for the perforated tubing, the probe rods were uncoupled from the expendable well point and hydraulically removed from the ground.

The temporary well points were allowed to stand for a period of one to five days to allow for groundwater recharge. Following this period, groundwater samples were collected with a peristaltic pump as described in Section 3.1.3.

Dedicated polyethylene tubing was used in each well point to minimize the potential for cross-contamination between sampling locations. In addition, the reusable probe rods were decontaminated prior to each use by scrubbing the rods in a solution of potable water and Alconox<sup>TM</sup> detergent. The rods were rinsed with potable water, followed by a final rinse with distilled water.

## 3.1.2 Well Point Locations and Depths

Groundwater samples were collected at thirty-five well point locations, as shown in Figure 3. Several of the actual well point locations differ slightly from the proposed locations presented in the Groundwater Monitoring Work Plan, based on accessibility restrictions caused by surface obstructions, subsurface obstructions, steep topography, or heavy vegetation. In addition, the locations of WP-5 and WP-21 have been approximated.

The well point locations were selected based on their proximity to the APCs described in the CAO, most of the which are relatively close to one another (i.e., PWTS, nitric acid concentrator units, loading and unloading areas, and portions of the plant drainage system). As these areas occupy a relatively small portion of the EDC facility (known as the Production Area), their areas of influence may actually overlap one another.

Well Point No.	Area of Potential Concern Targeted
1, 2, 3, 4	Background; along north property boundary
9, 11, 21, 35	Lake Kildeer Downstream Area
5, 6, 7, 19, 22	Lake Lee/Lake Kildeer Buffer Area
23, 24, 25, 26	Lake Lee Area
8, 10, 12, 13, 14, 15, 16, 17, 18	Lake Kildeer Area
20, 27, 28, 29	Nitrate truck and train loading areas
30, 31, 32, 33, 34	Acid concentrator units, acid loading areas

A listing of each well point location and its associated APC is presented below:

Depths of the well point installations ranged from approximately 12 feet below grade (at several locations in the vicinity of Lake Kildeer) to approximately 34 feet below grade (at upgradient location WP-1 along the northern property line). Installation depths were variable around the site based on topographic elevations, evidence of saturated conditions, and boring refusal in the subsurface. A summary of the well point investigation program, including the installation depth of each well point, is presented in Table 2.

## 3.1.3 Groundwater Level Measurements and Sample Collection

Following installation, each well point was allowed to recharge and equilibrate for a period of one to five days. A pressure manometer was used to determine the approximate depth to the groundwater surface within each well point. The manometer was attached to a section of 5/16'' diameter, dedicated polyethylene tubing which was placed inside the 3/8'' diameter

perforated well point tubing. The manometer registered a significant pressure change when it intercepted the static water level inside the 3/8" tubing. A marking was placed upon the smaller tubing prior to its removal from the well point tubing, and a tape measure was used to measure the approximate distance from the ground surface to the water level interface.

Following water level measurement, dedicated 5/16" polyethylene tubing ("extraction tubing") was placed inside the well point tubing for groundwater withdrawal. A piece of dedicated, flexible silicon tubing was placed on the end of the extraction tubing, and attached to a variable speed peristaltic pump for groundwater extraction. A volume of at least 40 milliliters (mLs) was purged from each well point prior to sample collection. At those locations where groundwater yield was sufficient, greater volumes were purged prior to sample collection. In general, increased purging resulted in a reduction in sample turbidity at these locations. However, a majority of the samples contained significant amounts of sediment in the sample bottles.

Samples were collected from the dedicated extraction tubing directly into laboratory-supplied sample containers. Samples for metals analysis were collected in bottles containing laboratory-supplied preservative (HNO<sub>3</sub>). The sample bottles were labeled, and packed in dry ice in a sample cooler. Samples were transported to the laboratory at the end of each day of sampling under chain-of-custody procedures.

Two blind duplicate samples and two field equipment rinsate samples were collected during the sampling program. Blind duplicate No. 1 was collected at upgradient location WP-2, while Blind Duplicate No. 2 was obtained at location WP-12, adjacent to Lake Kildeer. The field equipment rinsate samples were collected by pouring laboratory-supplied distilled water over and through decontaminated probe rods, and into laboratory-supplied sample containers. The field rinsate samples were collected following installation of well points WP-26 and WP-35, respectively.

#### 3.2 LABORATORY ANALYSES

Groundwater samples, blind duplicates and field equipment rinsate samples were analyzed by Arkansas Analytical, Inc. for the target parameters nitrate, sulfate, total lead, and total chromium, in accordance with the following table:

Parameter	Method	Container	Preservative	Holding Time
Nitrate	EPA 9200	125 mL Plastic	4°C	2 days
Sulfate	EPA 9038	125 mL Plastic	4°C	28 days
Lead	EPA 7421	125 mL Plastic	HN0 <sub>3</sub> & 4°C	6 months
Chromium	EPA 7190	125 mL Plastic	HN0 <sub>3</sub> & 4°C	6 months

Arkansas Analytical, Inc. is a state certified analytical testing laboratory. Laboratory results are discussed in Section 4.2, and the analytical data reports are presented in Appendix A.

#### 3.3 MONITORING NETWORK SURVEY

Following completion of the well point installations, a survey was conducted to establish horizontal and vertical locations of the sampling points. The survey was conducted by Ball & Paulus, Inc., an Arkansas Registered Professional Land Surveyor. Well locations are shown in Figure 3, and surveyed elevations are presented in Table 2.

The well point survey provided horizontal definition of the sampling points with respect to an established plant coordinate system, and vertical definition of the ground surface elevation (with respect to mean sea level) at each sampling location.

#### 3.4 BOREHOLE ABANDONMENT

Upon groundwater sampling and following completion of the well point survey, all temporary well points were abandoned by removing the perforated well point tubing and backfilling the one-inch diameter borehole to grade level with bentonite pellets. The bentonite pellets were hydrated with potable water to effectuate a thorough seal of the borehole.

## 4.1 GROUNDWATER ELEVATIONS AND FLOW DIRECTION

The Phase I groundwater investigation confirmed the presence of groundwater at each of the 35 well point locations. Although groundwater was not immediately present upon installation of several well points, the static groundwater level rose to near ground surface after several hours. The results of the water level survey indicate that groundwater observed during the Phase I investigation may exist under confined or semi-confined conditions at many of the well point locations. The results of the water level survey are summarized in Table 2. As pressure manometer measurements may be considered somewhat less accurate than more conventional methods for water level determination (e.g., electronic water level indicators used within a monitoring well), groundwater elevation data has been rounded to the nearest 0.1 feet.

Using the approximate groundwater elevations obtained during the water level survey, a contour map depicting a generalized groundwater flow direction was developed and is presented in Figure 5. The groundwater contour map identifies the general direction of groundwater flow over most of the EDC site to the east-southeast. Groundwater flow appears to be locally affected by ground surface topography, especially in the northeast portion of the site, where local groundwater flow direction appears to be toward the southwest. In addition, Lake Lee and Lake Kildeer locally affect groundwater flow direction in their respective vicinities.

## 4.2 ANALYTICAL RESULTS

The analytical results indicate that lead and chromium are present in the groundwater at relatively similar concentrations throughout the EDC site. In addition, several well point locations were found to exhibit elevated concentrations of nitrate and sulfate. The four locations installed along the northern property line (WP-1 through WP-4) were expected to be upgradient from plant activities and, therefore, presumably unaffected by potential site releases. The groundwater data obtained from these four upgradient locations indicates that lead and chromium concentrations are consistent with concentrations found throughout much of the EDC site.

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The results of the laboratory analytical program are discussed below and summarized in Table 3.

## 4.2.1 Lead

Lead was quantified in each of the groundwater samples obtained from the 35 well points, at concentrations ranging from 0.002 mg/L (WP-16 and WP-25) to 1.23 mg/L (WP-3). The average (mean) concentration was calculated at 0.109 mg/L, while the median concentration was calculated at 0.040 mg/L. Twenty-nine groundwater samples were quantified above the regulatory action level of 0.015 mg/L. In addition, three of the four upgradient (i.e., "background") well point locations were quantified with lead concentrations in excess of the regulatory action level. Concentrations in the background well points ranged from 0.011 mg/L at WP-2 to 1.23 mg/L at WP-3.

## 4.2.2 Chromium

Chromium was quantified in 20 of the 35 groundwater samples obtained during the well point investigation. Detected chromium concentrations ranged from 0.1 mg/L at WP-7 to 2.03 mg/L at WP-3. The average (mean) concentration was calculated at 0.259 mg/L, while the median concentration was calculated at 0.120 mg/L. Nineteen of the 35 groundwater samples were quantified at concentrations in excess of the USEPA MCL of 0.10 mg/L for chromium in drinking water. In addition, two of the four upgradient (i.e., background) well point locations were quantified with chromium concentrations in excess of the MCL. Concentrations in the background well points were 0.26 mg/L at WP-4 and 2.03 mg/L at WP-3.

## 4.2.3 Nitrate

Nitrate was quantified in 29 of the 35 groundwater samples, with detected concentrations ranging from 0.1 mg/L at WP-1 and WP-18, to 1,000 mg/L at WP-30. The average (mean) concentration was calculated at 62.8 mg/L, while the median concentration was calculated at 1.1 mg/L. Eight locations were quantified at concentrations in excess of the USEPA MCL of 10.0 mg/L for nitrate in drinking water. These locations included WP-9 (19.1 mg/L), WP-15 (94 mg/L), WP-16 (56 mg/L), WP-10 (220 mg/L), WP-28 (220 mg/L), WP-17 (224 mg/L), WP-31 (266 mg/L), and WP-30. Nitrate was not detected above the laboratory's Practical Quantification Limit (PQL) in upgradient WP-2, while the remaining upgradient locations were quantified at concentrations below 1.0 mg/L.

#### 4.2.4 Sulfate

Sulfate was quantified in 32 of the 35 groundwater samples, at concentrations ranging from 6 mg/L in WP-15 and WP-31, to 3,540 mg/L at WP-32. The average (mean) concentration was calculated at 248 mg/L, while the median concentration was calculated at 79 mg/L. Well points WP-29 (1,070 mg/L) and WP-32 were quantified at concentrations in excess of the proposed USEPA MCL of 500 mg/L for sulfate in drinking water. Sulfate was not detected above the laboratory PQL at upgradient locations WP-3 and WP-4, while upgradient locations WP-1 and WP-2 were quantified at 21 mg/L and 79 mg/L, respectively.

## 5.1 GROUNDWATER ELEVATION AND FLOW DIRECTION

Based on the results of the preliminary Phase I groundwater investigation, groundwater was encountered beneath the EDC site at depths ranging from near ground surface in many low-lying areas of the site, to approximately 22 feet below grade at the extreme northeast portion of the site. In general, groundwater flow beneath the site is to the east-southeast, with the exception of several areas locally influenced by ground surface topography and the presence of surface water bodies (i.e., Lake Lee and Lake Kildeer).

Several well points did not provide evidence of significant moisture immediately after installation. Groundwater was later observed near the ground surface in some of these locations. Therefore, is it believed that groundwater may exist under confined or semi-confined conditions at several locations around the EDC site.

## 5.2 GROUNDWATER QUALITY

As previously stated, a majority of the groundwater samples were turbid, and contained a significant layer of sediment upon settling. The sample turbidity could contribute to sample matrix interferences for total metals and/or increased total metals results. The average concentrations in soil for lead and chromium in the eastern United States are 17 mg/Kg and 52 mg/Kg, respectively (USGS, 1984). As the samples for total metals analysis were preserved with nitric acid to a pH of less than 2, the naturally occurring lead and chromium in soil would be leached over time from the soil into the acidic groundwater sample solution.

During the laboratory sample preparation, a representative aliquot of the sample is digested by adding more acid reagents to the sample and heating to aid in the process. Any sediments contained in the representative groundwater aliquot could contribute to the total lead and total chromium results. It should be noted that one of the samples with elevated total chromium and total lead contained approximately one-fourth sediment. This sample (WP-26) corresponded with elevated levels of 0.49 mg/L lead and 0.54 mg/L chromium.

For the next phase of the groundwater investigation, both filtered and unfiltered groundwater samples are proposed to be collected for analysis of dissolved and total metals, respectively.

## 5.2.1 Lead

Lead was quantified in each of the groundwater samples obtained during the Phase I investigation, including each of the four upgradient well points. No significant trend can be observed from the data produced during the Phase I investigation regarding the impact of site operations on lead concentrations in groundwater beneath the EDC site. It is anticipated that once groundwater monitoring wells are installed during Phase II activities, the lead concentrations will decrease due to decreased turbidity.

## 5.2.2 Chromium

Chromium was quantified in most of the groundwater samples obtained during the Phase I investigation. Similar to lead, the highest recorded chromium concentration was detected at an upgradient well point location. No significant trend can be observed from the data produced during the Phase I investigation regarding the impact of site operations on chromium concentrations in groundwater beneath the EDC site. Again, it is anticipated that once groundwater monitoring wells are installed during the Phase II activities, the chromium concentrations will decrease due to decreased turbidity.

#### 5.2.3 Nitrate

Elevated nitrate concentrations were observed in the vicinity of Lake Kildeer and the acid and nitrate process areas. Based on nitrate concentrations in excess of the USEPA MCL at eight well point locations, nitrate in groundwater remains a potential concern at these areas.

#### 5.2.4 Sulfate

Sulfate concentrations were relatively low and consistent throughout the EDC site, with the exception of one location near the acid process area (WP-32) and one location near the nitrate process area (WP-29). For the most part, sulfate is not considered a significant concern throughout the majority of the EDC site. However, its presence at elevated concentrations above the proposed USEPA MCL in the vicinity of the acid and nitrate process areas remains a potential concern.

## 5.3 PROPOSED AREAS FOR ADDITIONAL INVESTIGATION

The Phase I investigation identified six general vicinities which, based on elevated concentrations of one or more of the targeted parameters, warrant additional investigation. The six areas include:

- The northern portion of the EDC site in the vicinity of well point WP-3, which was quantified with elevated concentrations of lead and chromium.
- The area to the northwest and north of the EDC Production Area, in the vicinity of the Nitrate Truck and Train Loading Areas and the Acid Train Loading Area. This area is of concern based on the presence of elevated concentrations of lead (WP-27, WP-30, WP-31, WP-32), chromium (WP-32), nitrate (WP-28, WP-30, WP-31) and sulfate (WP-29, WP-32).
- The area north of Lake Lee, in the vicinity of well point WP-26, based on the presence of lead and chromium at elevated concentrations.
- The low-lying area along the dirt roadway leading to Lake Kildeer, in the vicinity of well point WP-5, based on the presence of lead and chromium at elevated concentrations.
- The area to the northwest of Lake Kildeer, based on the presence of elevated concentrations of nitrate (WP-15, WP-16, WP-17) and lead (WP-18).
- The area to the east-southeast of Lake Kildeer, based on the presence of nitrate (WP-10) and lead and chromium (WP-21) at elevated levels.

In order to address groundwater quality and flow direction in these areas, installation of groundwater monitoring wells in the uppermost saturated zone is recommended, as described in Section 6.0.

#### 6.0 RECOMMENDATIONS FOR ADDITIONAL INVESTIGATION

In order to further address groundwater quality and flow direction at several areas of potential concern at the EDC site, installation and sampling of groundwater monitoring wells are proposed, as described below.

#### 6.1 MONITORING WELL INSTALLATION

A total of eighteen (18) groundwater monitoring wells are proposed to be installed during the Phase II groundwater investigation. The monitoring wells will be installed to a depth of approximately 10 feet into the uppermost saturated unit, or to the top of a confining layer, whichever is encountered first. Based on field observations from the Phase I investigation and from previous investigations, it is assumed that the maximum well depth will not exceed 40 feet below grade.

The proposed monitoring well locations are presented in Figure 6.

## 6.1.1 Monitoring Well Construction

The groundwater monitoring wells will be constructed in accordance with USEPA guidance for well construction in overburden (unconsolidated) formations. It is anticipated that the monitoring wells will be drilled with a truck mounted drilling rig utilizing hollow stem augers.

The monitoring wells will be screened across the uppermost saturated zone utilizing ten feet of 4-inch diameter, 0.010-inch slotted polyvinyl chloride (PVC) well screen. The well casing will be constructed with 4-inch diameter PVC. The annular space around the well screen will be filled using No. 10/20 clean sand pack to a height of two feet above the top of the screen. A two foot thick seal of dry bentonite pellets will be placed above the sand pack, and hydrated with potable water. The remaining annular space will be filled with a bentonitecement grout mixture to a height of approximately 6-inches below grade. A schematic for a typical monitoring well construction is presented in Figure 7.

Each monitoring well will be secured with a water-tight locking cap and padlock. The monitoring wells will be finished within a steel protective manhole finished flush-to-grade, or within a steel protective casing finished approximately three feet above grade, depending on surrounding conditions. Each protective manhole and casing will be set in concrete.

#### 6.1.2 Soil Sampling

Soil samples will be collected at various intervals at each location for the purpose of determining subsurface lithology and depth of well screen placement. Samples will either be collected at 5-foot intervals using stainless-steel split spoon samplers, or continuously using a CME 5-foot core barrel. All soil samples will be logged according to the Unified Soil Classification System, and selected samples may be retained for laboratory geotechnical analyses, as appropriate based on field observations. Woodward-Clyde field personnel will perform visual screening of each sample collected and record observations relating to sample recovery, color, density, moisture content, homogeneity, presence of odor or staining, and blow counts. Observations will be recorded in a bound field log book.

#### 6.1.3 Decontamination

All downhole drilling equipment (e.g., drill bits, augers) will be decontaminated between each location by high pressure washing. Downhole sampling equipment (e.g., split-spoon samplers, Shelby tubes, CME core barrel, water level probes) will be decontaminated using a solution of non-phosphate detergent in potable water, followed by a rinse with clean, potable water. Wash water resultant from decontamination procedures will be containerized for characterization and proper disposal by EDC.

#### 6.1.4 Well Development

After allowing the well materials to set for at least 24 hours, each monitoring well will be developed by pumping or surge blocking and bailing until field parameters (i.e., pH, conductivity, temperature) stabilize and the well produces a clear discharge. Development water resultant from the field program will be contained in 55-gallon DOT drums for characterization and proper disposal by EDC.

## 6.2 MONITORING WELL SURVEY

Following installation, each monitoring well will be surveyed for location and elevation by an Arkansas Registered Professional Land Surveyor. Elevation measurements will be conducted to the nearest 0.1 feet above msl at the base of each monitoring well, and to the nearest 0.01 feet above msl at the top of casing (TOC) at each well. A permanent marking will be inscribed at the location of each TOC measurement for future reference. A surveyed plot plan will be prepared presenting the location of each well relative to the monitoring well network and to relevant site structures (e.g., lakes, production and loading areas, etc.)

#### 6.3 GROUNDWATER SAMPLING

#### 6.3.1 Groundwater Elevations

Groundwater samples will be collected from each well at least two weeks after well development. Prior to sample collection, depth to water measurements will be obtained at each well location using an electronic water level indicator. The depth to water will be measured from the TOC and recorded to the nearest 0.01 feet. Depth to water measurements will be referenced to the respective TOC elevations, and static groundwater elevations will be calculated for each well location. To minimize the potential for cross-contamination, the water level indicator will be decontaminated between sample locations as described in Section 6.1.3.

#### 6.3.2 Sample Collection

Following water level measurements, the volume of water within each well will be calculated using the following formula:

[Total Well Depth (ft.) - Depth to Water (ft.)]  $\times 0.653 =$  Gallons of water in casing

Prior to sampling, a minimum of three times the volume of standing water in the well will be purged by hand bailing or pumping. Purge water will be containerized for characterization and proper disposal. After purging, each well will be allowed to recharge to at least 80% of its original static water level, or for two hours, whichever occurs sooner.

Upon allowing each well to recharge, groundwater samples will be collected utilizing laboratory-cleaned, dedicated, disposable polyethylene bailers. Samples will be transferred into laboratory-supplied clean glassware, with laboratory-prepared preservatives, as appropriate. Field meters will be used to record pH, conductivity, temperature, and turbidity at each monitoring well during the sampling program.

Information such as sampling times, purge volumes, weather conditions, and field parameter concentrations will be recorded in the field during sampling on Woodward-Clyde's Groundwater Sampling Record Sheets.

#### 6.3.3 Laboratory Analysis

Samples will be analyzed by an Arkansas-certified analytical laboratory, in accordance with the analytical program outlined in Table 4.

Parameter	Method
Lead (total)	SW-846 / EPA 7421
Lead (dissolved)	SW-846 / EPA 7421
Chromium (total)	SW-846 / EPA 6010 or 7190
Chromium (dissolved)	SW-846 / EPA 6010 or 7190
Nitrate	SW-846 / EPA 9200 or 9056
Sulfate	SW-846 / EPA 9038 or 9056

Proposed analytical methods for each of the parameters are shown on the following table:

Field quality assurance/quality control (QA/QC) samples will include one field blank per day of sampling, and one blind duplicate sample for the sampling event. The field blank is collected to confirm that contaminants have not been introduced into the groundwater samples by the sampling method. The field blank will be collected by pouring laboratorysupplied analyte-free water through a sampling bailer and into laboratory-supplied sample containers. The blind duplicate sample is a duplicate of a groundwater sample collected at a specific well, and submitted to the laboratory without designating the sample origin. The results of the blind duplicate sample can be compared to the results of the original groundwater sample to provide an indication of the reproducibility of the laboratory's analytical and reporting procedures. The field blank and blind duplicate samples will be analyzed for each of the parameters in the above table.

Laboratory QA/QC will include reagent blanks, matrix spikes, total recoverables, spiking concentrations, and laboratory quality control samples.

Waste characterization samples will be collected from the drums of decontamination water and well purging water, as well as from the drummed drill cuttings. Composite samples will be submitted for analysis of total lead, total chromium, nitrate and sulfate, as appropriate. Each waste stream will be properly disposed of based on the results of the waste characterization.

#### 6.4 MONITORING WELL/PIEZOMETER DECOMMISSIONING

While the drilling contractor is mobilized at the EDC site, sixteen of the existing monitoring wells and piezometers installed during previous site investigations will be properly abandoned due to the fact that there are no records on how they were installed. The wells to be abandoned include 12 locations around Lake Kildeer (identified as Piezometers A through F, and monitoring wells 1, 2, 2A, 3, 4, and 5), and 4 locations around Lake Lee (identified as L-1 through L-4). The wells and piezometers will be properly abandoned according to Arkansas Water Well Commission guidelines by a licensed water well driller.

The wells and piezometers will be properly abandoned by overdrilling and removing the well screen and casing, and filling the borehole to grade with a bentonite-cement grout. Grout will be applied directly to the bottom of the borehole using a tremie pipe to prevent bridging.

As an alternative, the wells may be cut flush to grade and abandoned in place by filling the well screen and casing with a bentonite-cement grout.

#### 6.5 SUMMARY REPORT

Following installation and sampling of the monitoring well network, a summary report will be developed which presents the results of the Phase II groundwater investigation. The report will include the following:

- Description of field activities relating to monitoring well installation and sampling
- Boring Logs for each borehole
- Well Construction Diagram for each monitoring well
- Groundwater Sampling Record Sheets with results of field measurements
- Analytical results of groundwater sampling program in tabular form
- Analytical data reports from laboratory
- Surveyed plot plan displaying location of monitoring well network relative to site structures
- Groundwater elevation contour map depicting groundwater flow regimes
- Concentration isopleths, as appropriate
- Recommendations for additional study, as warranted

It is anticipated that the Phase II investigation will more accurately define the site conditions with respect to groundwater quality and flow direction.

7.0 SCHEDULE

Woodward-Clyde will commence with field activities within three weeks after ADPC&E approval of this plan. Woodward-Clyde anticipates that a final report can be delivered to the ADPC&E within 120 days after written approval.

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TABLES

#### TABLE 1

#### DESCRIPTION OF HYDROGEOLOGIC UNITS IN THE STUDY AREA

System	Series	Group	Formation	Hydrogeologic Unit	Hydrogeologic Properties
Quaternary	Holocene and Pleistocene		Alluvial and terrace deposits		Clay, silt, sand, and gravel. Present only in bottomlands of most streams. Generally not used. As much as 100 feet thick.
			Cockfield Formation	Cockfield aquifer	Lignitic sand with interbedded clay. Principal aquifer for rural domestic supply. Water withdrawls approximately 0.5 million gallons per day. Approximately 200 feet thick where present.
			Cook Mountain Formation	Cook Mountain confining unit	Clay with interbedded fine sand. Not an aquifer. Thickness ranges from 50 to 200 feet.
Tertiary	Eocene	Claiborne	Sparta Sand	Greensand aquifer	Thinly bedded fine glauconitic sand with interbedded clay. Source of municipal and industrial water supply principally in southeast part of county. Water withdrawals approximately 0.5 million gallons per day. Approximately 200 feet thick.
				Middle confining unit	Clay and silt. Not an aquifer. Thickness ranges from 40 to 160 feet.
				El Dorado aquifer	Thickly bedded medium to coarse sand. Source of municipal and industrial water supply throughout the county. Water withdrawals approximately 14 million gallons per day. Approximately 300 feet thick.
			Cane River Formation	Cane River confining unit	Clay and silty clay. Not an aquifer. Approximately 300 feet thick.

#### Table 2 Summary of Well Point Data Phase I Hydropunch Investigation El Dorado Chemical Company November 1995

Well	Total	Depth to	Ground	Groundwater
Point No.	Depth (ft.)	Water (ft.)	Elevation (ft. MSL)	Elevation (ft. MSL)
WP-1	34.5	15.2	206.7	191.5
WP-2	27.0	4.7	190.6	185.9
WP-3	24.0	1.7	181.9	180.2
WP-4	27.5	3.5	210.8	207.3
WP-5	32.0	1.5	200.9	199.4
WP-6	23.0	17.3	201.8	184.5
WP-7	27.0	2.4	171.2	168.8
WP-8	30.5	13.0	182.3	169.3
WP-9	21.0	14.7	168.5	153.8
WP-10	18.0	14.5	174.8	160.3
WP-11	19.5	12.3	176.7	164.4
WP-12	12.0	4.5	173.1	168.6
WP-13	12.0	4.2	175.2	171.0
WP-14	12.0	0.5	172.9	172.4
WP-15	12.0	3.5	175.4	171.9
WP-16	12.0	5.5	178.4	172.9
WP-17	12.0	7.7	176.0	168.3
WP-18	12.0	7.6	173.9	166.3
WP-19	27.0	21.6	212.1	190.5
WP-20	20.0	7.1	172.6	165.5
WP-21	24.0	4.9	149.7	144.8
WP-22	22.0	11.2	166.4	155.2
WP-23	21.0	6.1	163.2	157.1
WP-24	21.0	7.9	161.8	153.9
WP-25	21.0	11.2	163.9	152.7
WP-26	21.0	6.6	182.0	175.4
WP-27	26.0	3.0	199.9	196.9
WP-28	23.0	14.7	202.8	188.1
WP-29	25.0	8.9	196.3	187.4
WP-30	24.0	10.5	194.5	184.0
WP-31	22.0	4.8	188.2	183.4
WP-32	30.0	17.2	195.8	178.6
WP-33	24.0	7.9	198.0	190.1
WP-34	15.0	17.0	199.0	182.0
WP-35	12.0	0.5	162.2	161.7

#### Table 3 Summary of Groundwater Quality Data Phase I Groundwater Investigation El Dorado Chemical Company El Dorado, Arkansas November 1995

Well Point	Lead	Chromium	Nitrate	Sulfate
No.	(mg/L)	(mg/L)	(mg/L)	(mg/L)
1	0.021	<0.08	0.1	21
2	0.011	<0.08	<0.1	79
3	1.23	2.03	0.98	<50
4	0.063	0.26	0.79	<50
5	0.301	0.61	0.24	353
6	0.062	0.16	9.6	363
7	0.044	0.1	<0.1	49
8	0.035	<0.08	<0.1	15
9	0.03	<0.08	19.2	172
10	0.03	<0.08	220	9
11	0.025	0.12	4.15	335
12	0.011	<0.08	1.26	176
13	0.046	0.15	1.9	20
14	0.03	0.17	1.8	12
15	0.038	<0.08	94	6
16	0.002	<0.08	56	8
17	0.01	< 0.08	224	15
18	0.098	0.18	0.1	32
19	0.052	< 0.08	0.18	<2
20	0.05	0.16	1.32	159
21	0.31	0.79	<0.1	163
22	0.012	<0.08	<0.1	7
23	0.04	0.11	0.22	267
24	0.016	<0.08	0.28	216
25	0.002	< 0.08	0.2	208
26	0.49	0.54	0.47	139
27	0.09	0.21	0.73	145
28	0.036	0.12	220	357
29	0.044	0.18	3.4	1070
30	0.192	0.35	1000	89
31	0.082	0.23	266	6
32	0.196	0.75	0.68	3540
33	0.04	<0.08	<0.1	54
34	0.058	0.12	5.4	470
35	0.028	<0.08	1.12	14
Action Level	0.015 <sup>A</sup>	0.100 <sup>B</sup>	10.0 <sup>B</sup>	500 <sup>C</sup>

Notes: <sup>A</sup> - USEPA action level for lead.

<sup>B</sup> - USEPA MCL.

<sup>C</sup> - Proposed USEPA MCL.

# Table 4Summary of Proposed Analytical ProgramPhase II Groundwater InvestigationEl Dorado Chemical Company

Monitoring				
Well No.	Lead <sup>A</sup>	Chromium <sup>B</sup>	Nitrate <sup>C</sup>	Sulfate <sup>D</sup>
MW-EDC-1	Х	X		
MW-EDC-2	Х	X		
MW-EDC-3	Х	X		
MW-EDC-4	Х	X	X	X
MW-EDC-5	Х	X		X
MW-EDC-6	Х	X	X	X
MW-EDC-7	Х	X	X	
MW-EDC-8	Х	X	X	
MW-EDC-9	Х	X		X
MW-EDC-10	Х	X	X	
MW-EDC-11	Х	X		
MW-EDC-12	Х	X		
MW-EDC-13	Х	X		
MW-EDC-14	X	X	X	
MW-EDC-15	Х	X	X	
MW-EDC-16	Х	X	X	
MW-EDC-17	X		X	
MW-EDC-18	X	X		

Notes:

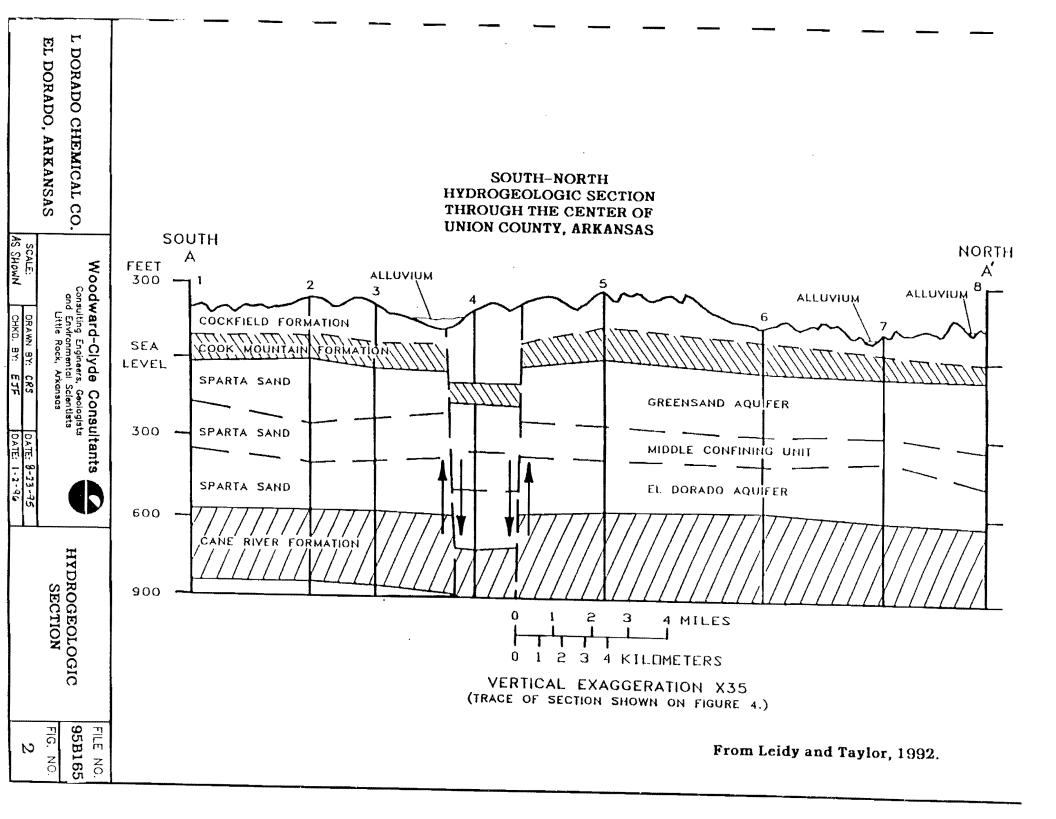
<sup>A</sup> - Total and dissolved lead by Method SW-846/EPA 7421.

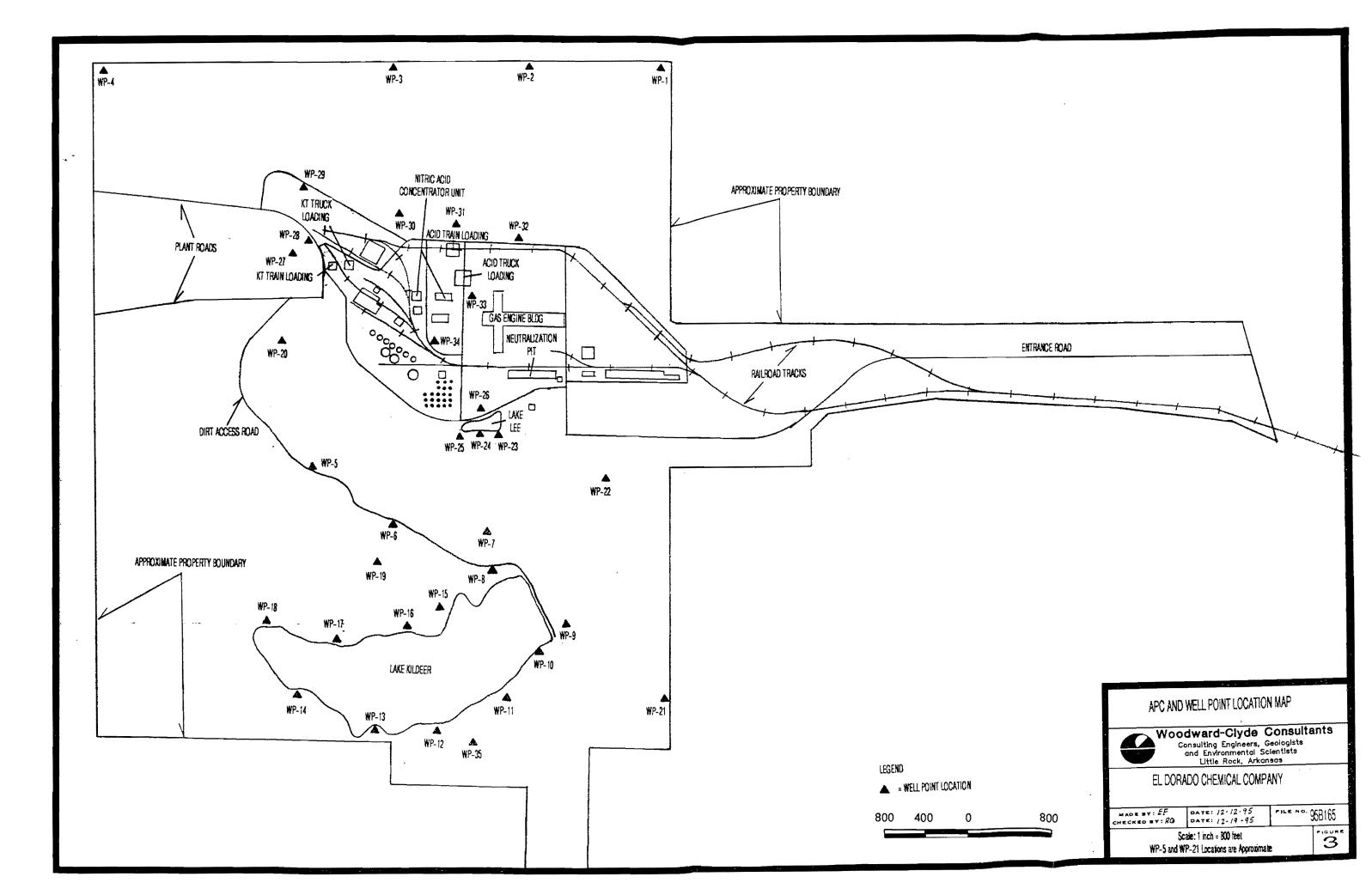
<sup>B</sup> - Total and dissolved chromium by Method SW-846/EPA6010 or 7190.

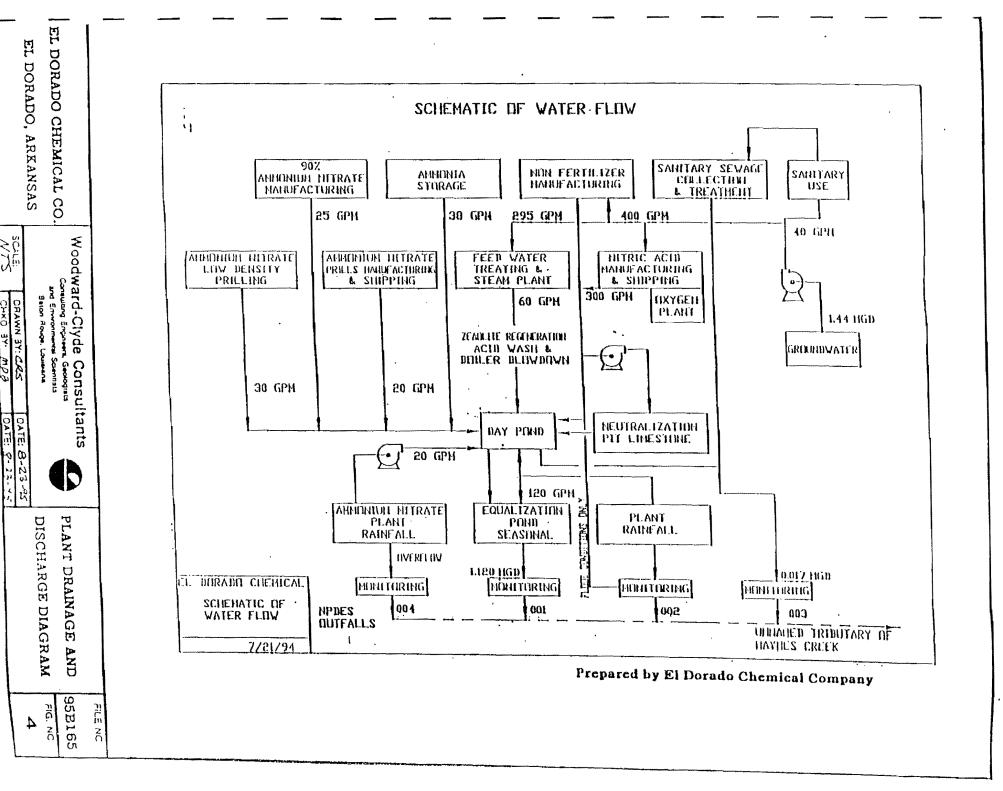
<sup>C</sup> - Nitrate by Method SW-846/EPA 9200 or 9056.

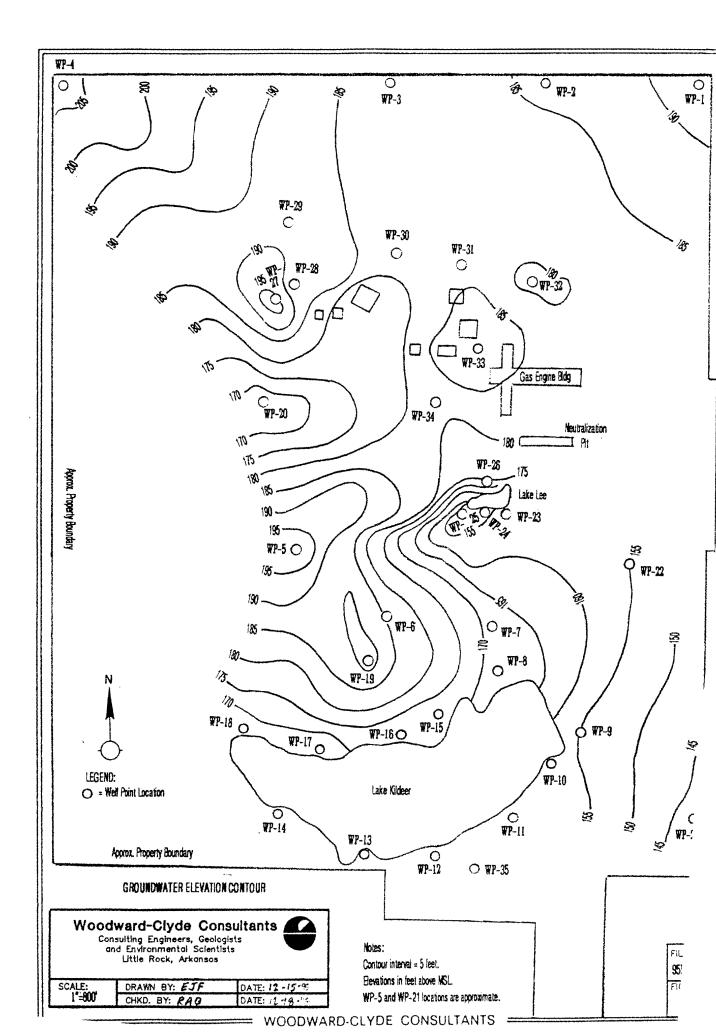
<sup>D</sup> - Sulfate by Method SW-846/EPA 9038 or 9056.

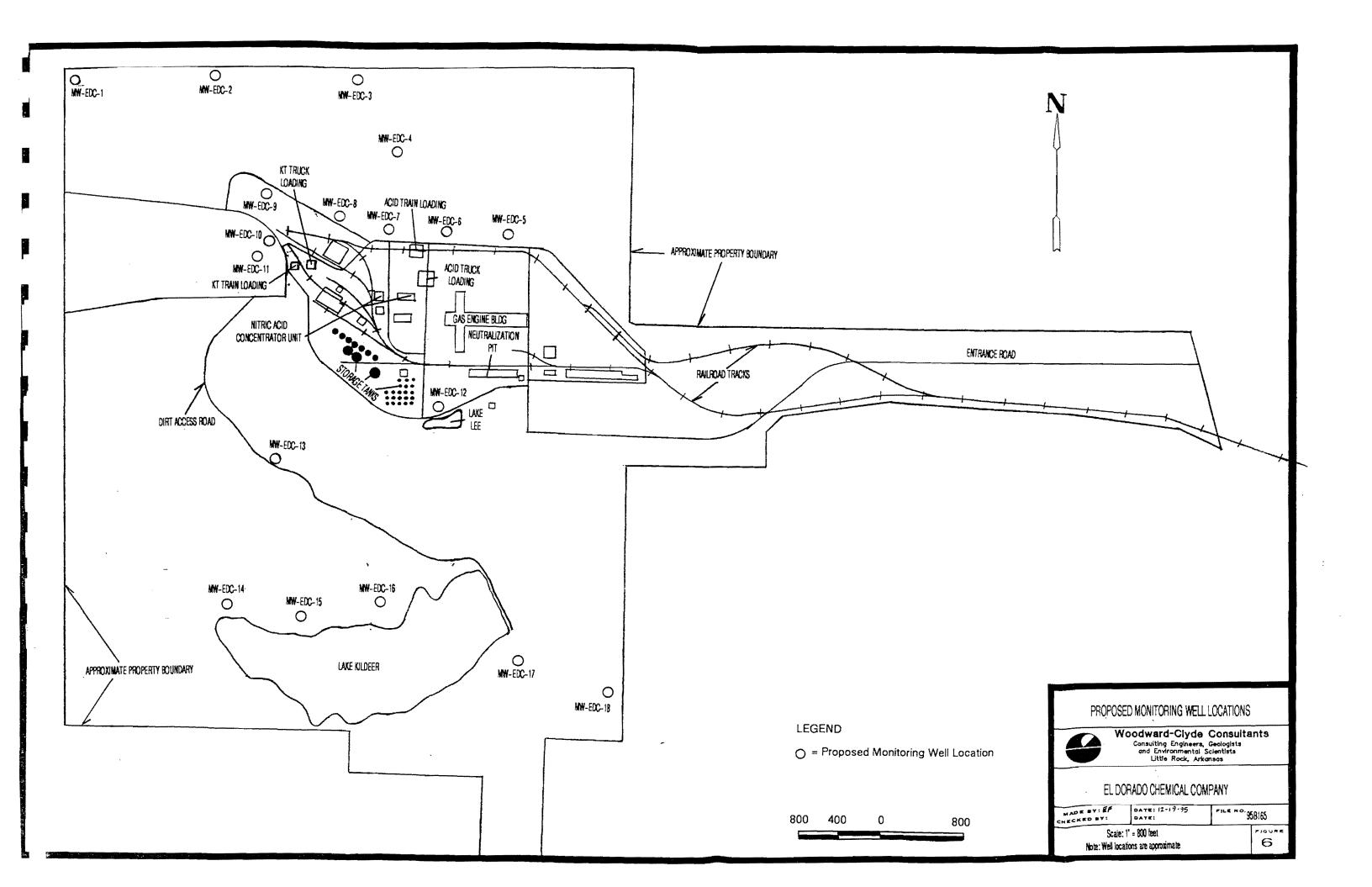
FIGURES

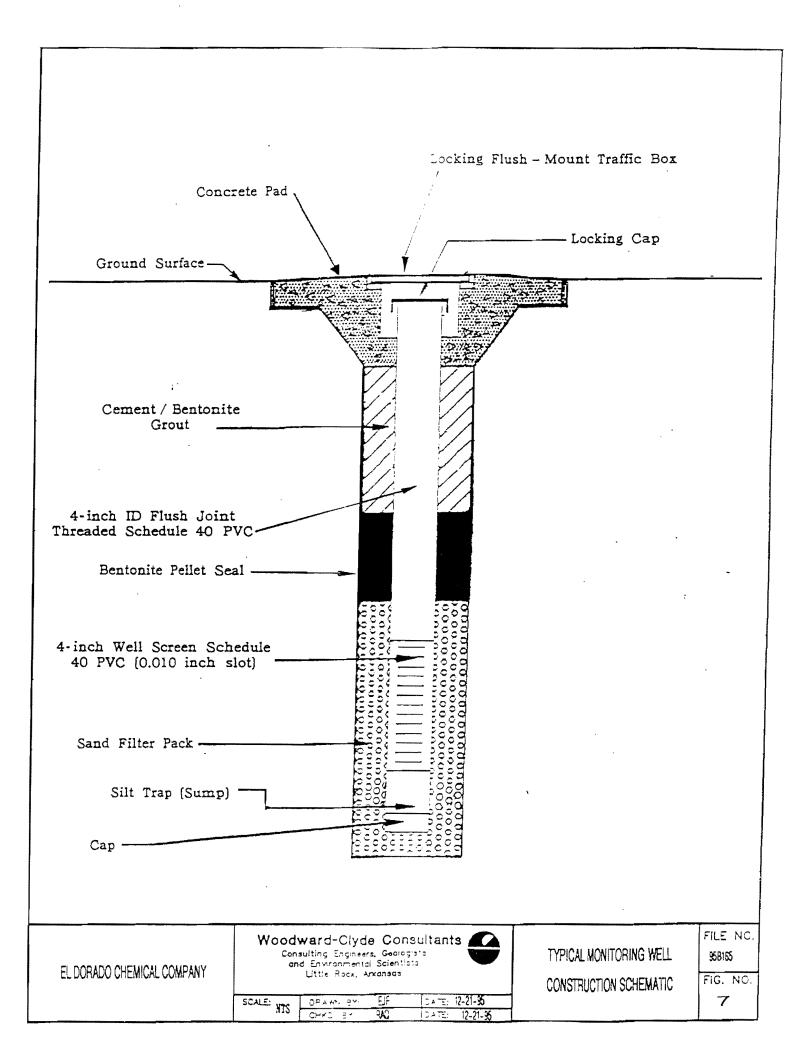












### APPENDIX A ANALYTICAL RESULTS

#### 07-Dec-95

Woodward-Clyde Consultants 900 S. Shackleford Little Rock, Arkansas 72211 Re: El Dorado Chemical Project: GW INV Phase I

Date Received: 11/16-17/95

#### Attn: Eric Fox

ANALYTICAL RESULTS	
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	Lab	Date	Sample	Sample			Nitrates	Sulfates	
=	Number	Sampled	Туре	1D	mg/L	mg/L	mg/L	mg/L	
	952316	11-16-95	water	WP-1	0.021	<0.08	0.1	21	
	952317	11-16-95	water	WP-2	0.011	<0.08	<0.1	79	
	952318	11-16-95	water	WP-7	0.044	0.1	<0.1	49	
	952319	11-16-95	water	WP-8	0.035	<0.08	<0.1	15	
	952320	11-16-95	water	WP-9	0.03	<0.08	19.2	172	
	952321	11-16-95	water	WP-11	0.025	0.12	4.15	335	
	952322	11-16-95	water	WP-12	0.011	<0.08	1.26	176	
	952308	11-16-95	water	WP-13	0.046	0.15	1.9	20	
	952323	11-16-95	water	WP-14	0.038	0.17	1.8	12	
	952324	11-16-95	water	WP-15	0.030	<0.08	94	6	
	952325	11-16-95	water	WP-16	0.002	<0.08	56	8	
	952307	11-16-95	water	WP-17	0.01	<0.08	224	15	
	952306	11-16-95	water	WP-18	na	na	0.1	32	
	952314	11-16-95	water	WP-27	0.09	0.21	0.73	145	
	952358	11-17-95	water	WP-21	0.31	0.79	<0.1	163	
	952359	11-17-95	water	WP-22	0.012	<0.08	<0.1	7	
	952360	11-17-95	water	WP-23	0.04	0.11	0.22	267	
	952361	11-17-95	water	WP-24	0.016	<0.08	0.28	216	
	952362	11-17-95	water	WP-25	0.002	<0.08	0.2	208	
	952363	11-17-95	water	WP-26	0.49	0.54	0.47	139	

Woodward-Clyde Consultants 900 S. Shackleford Little Rock, Arkansas 72211 Re: El Dorado Chemical Project: GW INV Phase I Date Received: 11/16-17/95

Attn: Eric Fox

ALTIN	AL RESULT	0			e ten 1. A re-Citation		
Lab	Date	Sample	Sample	Lead	Chromium	Nitrates	Sulfates
Number	Sampled	Туре	ID	mg/L	mg/L	mg/L	mg/L
952364	11-17-95	water	WP-33	0.04	<0.08	<0.1	54
952365	11-17-95	water	WP-20	0.05	0.16	1.32	159
952366	11-17-95	water	WP-18	0.098	0.18	na	na
952367	11-17-95	water	WP-10	0.03	<0.08	220	9
952368	11-17-95	water	WP-6	0.062	0.16	9.6	363
952369	11-17-95	water	WP-19	0.052	<0.08	0.18	<2
952370	11-17-95	water	WP-5	0.301	0.61	0.24	353
952371	11-17-95	water	WP-34	0.058	0.12	5.4	470
952372	11-17-95	water	WP-3	1.23	2.03	0.98	<50*
952373	11-17-95	water	WP-4	0.063	0.26	0.79	<50*
952313	11-16-95	water	WP-28	0.036	0.12	220	357
952312	11-16-95	water	WP-29	0.044	0.18	3.4	1070
952309	11-16-95	water	WP-30	0.192	0.35	1000	89
952310	11-16-95	water	WP-31	0.082	0.23	266	6
952311	11-16-95	water	WP-32	0.196	0.75	0.68	3540
952327	11-16-95	water	BLIND DUP #1	0.014	<0.08	<0.1	75
952328	11-16-95	water	BLIND DUP #2	0.005	<0.08	1.26	178
<del>9</del> 52326	11-16-95	water	WP-35	0.028	<0.08	1.12	14
952277	11-15-95	water	Field Blank 1	<0.001	<0.08	<0.1	9
952278	11-15-95	water	Field Blank 2	<0.001	<0.08	<0.1	7

\*Elevated detection limit due to dilution required to overcome interference.

#### 07-Dec-95

Woodward-Clyde Consultants 900 S. Shackleford Little Rock, Arkansas 72211

Attn: Eric Fox

QUALITY CONTROL RESULTS Percent Percent EPA Percent Recovery Recovery SW-846 Method of mg/L Variance Matrix Control Blank Spike/s Spike/s **Duplicates** Analysis Lead <0.001 6.6 99.5 97.7 7421 < 0.001 8.2 92.4 96.2 < 0.001 2.7 90.6 99.3 Chromium < 0.08 3.5 93.8 89 7190 < 0.08 1.6 94.2 91 <0.08 1.2 90.6 95.1 Nitrates < 0.1 5.3 120 113 9200 5.3 87.6 113 9 < 0.1 96.6 0 Sulfates 79.8 <1 116 9038 <1 3.8 93.8 106

Rodney J. Williams, Liz Potts, Tracy Bounds Analyzed by:

Re: El Dorado Chemical

Project: GW INV Phase I

Date Received: 11/16-17/95

Lessie R. Redican (ng) Man Lessie R. Redican, Norma J. James Reviewed by:

cc:

John Carver El Dorado Chemical Company P.O. Box 1373 Oklahoma City, Oklahoma 73101

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4	NP-23				830	,		23		2	3	8			
h	P-24				84	2		23	61_	2	X	X			
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	WP - 18				102	8			66	1		X		1	
	WP-10				1724				67	2	X	K		1	
	WP -6				133	3		23	368	2	X	X		1	
	WP-19				1348		Í		69	2	X	X		1	
	WP-5				1410				370	12	X			1	
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Woodward-Clyde Consultants

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Woodward-Clyde Consultants



CHAIN	-	OF	-	CUST	DDY	RECO	RD
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### APPENDIX D ANALYTICAL RESULTS

Client Name	Client Name: WOODWARD CLYDE CONSULTANTS-LITTLE ROCK 900 SOUTH SHACKLEFORD SUITE 412 LITTLE ROCK, AR 72211								
Client ID:	MW - 1	Pro	ject ID:	EL DORADO	CHEMICAL				
SWLO ID:	24948.10	Rep	ort:	24948.10					
Collected: Received:		Report Date: Last Modified:	03/27/1996	Page: Matrix:	1 Water				

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	date Analyzed	METHOD REFERENCE	
		*** INORG	ANICS ***				
NITRATE		0.2	mg/l	1.7	03/15/96	SW 9056	
SULFATE		0.2	mg/l	4.1	03/15/96	SW 9056	
		*** MET	ALS ***				
CHROMIUM		5.0	ug/l	ND	03/26/96	SW 6010	
LEAD		2.0	ug/l	3.7	03/21/96	SW 7421	

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
- = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE
- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = EPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	Client Name: WOODWARD CLYDE CONSULTANTS-LITTLE ROCK 900 SOUTH SHACKLEFORD SUITE 412 LITTLE ROCK, AR 72211									
Client ID:	MW-1-F	Pr	oject ID:	EL DORADO	CHEMICAL					
SWLO ID:	24948.20	Re	port:	24948.20						
Collected: Received:		Report Date: Last Modified:		Page: Matrix:	1 Water					

	DATE	DETECTION			DATE	METHOD	
TEST	EXTRACTED	LIMIT	UNITS	RESULTS	ANALYZED	REFERENCE	
		*** MB:	TALS ***				
CHROMIUM		5.0	ug/l	ND	03/27/96	SW 6010	
LEAD		2.0	ug/l	ND	03/21/96	SW 7421	×

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
- = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE
- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = BPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	900 SOUTH S SUITE 412	LITTLE ROCK, AR 72211								
Client ID:	MW-2	Pi	oject ID:	EL DORADO	CHEMICAL					
SWLO ID:	24948.11	Re	port:	24948.11						
Collected: ( Received: (		Report Date: Last Modified:	03/27/1996	5 Page: Matrix:	1 Water					

<u>TBST</u>	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	Method Reference		
*** INORGANICS ***								
NITRATE		0.2	mg/l	ND	03/15/96	SW 9056		
SULFATE		0.2	mg/l	17.0	03/15/96	SW 9056		
		*** MBT.	ALS ***					
CHROMIUM		5.0	ug/l	34.2	03/26/96	SW 6010		
LEAD		2.0	ug/l	18.0	03/25/96	SW 7421		

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
  - = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #BPA600/4-79-020, MARCH 1985
- \* SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

SW = EPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	900 SOUTH S SUITE 412	OODWARD CLYDE CONSULTANTS-LITTLE ROCK 900 SOUTH SHACKLEFORD UITE 412 ITTLE ROCK, AR 72211									
Client ID:	MW-2-F	Pro	oject ID:	EL DORADO	CHEMICAL						
SWLO ID:	24948.21	Rej	port:	24948.21							
Collected: Received:	03/14/1996 03/15/1996	Report Date: Last Modified:		5 Page: Matrix:	1 Water						

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	Method Reference			
*** METALS ***									
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	ND ND	03/27/96 03/21/96	SW 6010 SW 7421			

.D = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
  - = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

SW = EPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	Client Name: WOODWARD CLYDE CONSULTANTS-LITTLE ROCK 900 SOUTH SHACKLEFORD SUITE 412 LITTLE ROCK, AR 72211									
Client ID:	MW - 3	Pr	oject ID:	EL DORADO	CHEMICAL					
SWLO ID:	24948.12	Re	port:	24948.12						
Collected: Received:		Report Date: Last Modified:		Page: Matrix:	1 Water					

<u>TEST</u>	DATB BXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	METHOD REFERENCE		
*** INORGANICS ***								
NITRATE		0.2	mg/l	ND	03/15/96	SW 9056		
SULFATE		0.2	mg/l	10.0	03/15/96	SW 9056		
		*** MBT.	ALS ***					
CHROMIUM		5.0	ug/l	ND	03/26/96	SW 6010		
LEAD		2.0	ug/l	2.7	03/21/96	SW 7421		

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

- = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE
- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #BPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = BPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCI	x	
Client ID:	MW-3-F	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24948.22	Re	port:	24948.22	
Collected: Received:		Report Date: Last Modified:		5 Page: Matrix:	1 Water

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	METHOD REFERENCE	
*** METALS ***							
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	ND ND	03/27/96 03/22/96	SW 6010 SW 7421	

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
- : = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

IA = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = BPA METHODOLOGY, \*#SW846\*, THIRD EDITION, NOVEMBER 1986

Client Name	: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCH	ζ	
Client ID:	MW - 4	Pz	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24948.13	Re	port:	24948.13	
Collected: Received:	03/14/1996 03/15/1996	Report Date: Last Modified:	03/27/1996	Fage: Matrix:	1 Water

	DATE	DETECTION			DATE	METHOD	
TEST	EXTRACTED	LIMIT	UNITS	RESULTS	ANALYZED	REFERENCE	
		*** INORG	ANICS ***				
NITRATE		0.2	mg/l	1.3	03/15/96	SW 9056	
SULFATE		2.0	mg/l	728	03/19/96	SW 9056	
		*** MBT.	ALS ***				
CHROMIUM		5.0	ug/l	ND	03/26/96	SW 6010	
LEAD		2.0	ug/l	2.5	03/21/96	SW 7421	

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
- = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE
- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #BPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = EPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name		YDE CONSULTANTS- SHACKLEFORD , AR 72211	LITTLE ROCK	:	
Client ID:	MW - 4 - F	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24948.23	Rej	port:	24948.23	
Collected: Received:		Report Date: Last Modified:		Page: Matrix:	1 Water

<u>TEST</u>	date <u>extract</u> ed	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	Method Reference		
*** MBTALS ***								
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	ND ND	03/27/96 03/22/96	SW 6010 SW 7421		

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

- = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE
- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = EPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	900 SOUTH S SUITE 412	WOODWARD CLYDE CONSULTANTS-LITTLE ROCK 900 SOUTH SHACKLEFORD SUITE 412 LITTLE ROCK, AR 72211					
Client ID:	MW - 5	Projec	t ID: EL	DORADO	CHEMICAL		
SWLO ID:	24931.11	Report	: 24	931.11			
Collected: Received:		Report Date: 03/ Last Modified:		Page: Matrix:	1 Water		

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	METHOD REFERENCE	
		*** INORG	ANICS ***				
NITRATE		0.2	mg/l	4.4	03/14/96	SW 9056	
SULFATE		2.0	mg/l	441	03/15/96	SW 9056	
*** METALS ***							
CHROMIUM		5.0	ug/l	ND	03/19/96	SW 6010	
LRAD		2.0	ug/l	ND	03/21/96	SW 7421	

 $\omega$  = not detected above quantitation limit

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
  - = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

1 = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = EPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	2: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCK		
Client ID:	MW - 5 - F	Pro	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.27	Rer	port:	24931.27	
Collected: Received:		Report Date: Last Modified:	03/27/1996	Page: Matrix:	1 Water

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	Method Reference
		*** MBTI	112 ***			
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	ND ND	03/19/96 03/21/96	SW 6010 SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE - UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

- A = NOT APPLICABLE
- Methodology: SM \* STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = BPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	SUITE 412 LITTLE ROCK,		ITTLE ROCK		
Client ID:	MW - 6	Pro	ject ID: H	EL DORADO	CHEMICAL
SWLO ID:	24931.12	Rep	ort: 2	24931.12	
Collected: Received:		Report Date: Last Modified:	03/27/1996	Page: Matrix:	1 Water

	DATE	DETECTION			DATE	METHOD
TEST	EXTRACTED	LIMIT	UNITS	RESULTS	ANALYZED	REFERENCE
		*** INORG	ANICS ***			
NITRATS		2.0	mg/l	51.1	03/15/96	SW 9056
SULFATE		0.2	mg/l	24.0	03/14/96	SW 9056
		*** MBT.	ALS ***			
CHROMIUM		5,0	ug/l	ND	03/19/96	SW 6010
LEAD		2.0	ug/l	2.6	03/21/96	SW 7421

.D = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

= UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #BPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = BPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCK		
Client ID:	MW - 6 - F	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.28	Re	port:	24931.28	
Collected: Received:		Report Date: Last Modified:	03/27/1996	Page: Matrix:	1 Water

	DATE	DETECTION			DATE	METHOD
TEST	EXTRACTED	LIMIT	UNITS	RESULTS	ANALYZED	REFERENCE
		*** MBT	ALS ***			
CHROMIUM		5.0	ug/l	ND	03/19/96	SW 6010
LEAD		2.0	ug/l	ND	03/21/96	SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

= UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #BPA600/4-79-020, MARCH 1985
- \* SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	E: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		TTLE ROCK		
Client ID:	MW - 7	Proje	ect ID: EL	DORADO CHE	MICAL
SWLO ID:	24931.13	Repor	rt: 249	931.13	
Collected: Received:		Report Date: 03 Last Modified:		Page: Matrix: Wat	l er

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RBSULTS	DATE ANALYZED	METHOD REFERENCE
		*** INORG	ANICS ***			
NITRATE		2.0	mg/l	282	03/15/96	SW 9056
SULFATE		2.0	mg/l	380	03/15/96	SW 9056
		*** MB1	ALS ***			
CHROMIUM		5.0	ug/l	7.8	03/19/96	SW 6010
LEAD		2.0	ug/l	22.1	03/21/96	SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985

- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = BPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	E: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCH	ζ	
Client ID:	MW-7-F	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.29	Re	port:	24931.29	
Collected: Received:	03/13/1996 03/14/1996	Report Date: Last Modified:		Page: Matrix:	1 Water

	DATE	DETECTION			DATE	METHOD
TEST	EXTRACTED	LIMIT	UNITS	RESULTS	ANALYZED	REFERENCE
		*** MET	ALS ***			
CHROMIUM		5.0	ug/l	ND	03/19/96	SW 6010
LEAD		2.0	ug/l	18.5	03/21/96	SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

= UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE

Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #EPA600/4-79-020, MARCH 1985

- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	SUITE 412 LITTLE ROCK		LITTLE ROCI	x	
Client ID:	MW - 8	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.14	Re	port:	24931.14	
Collected: Received:		Report Date: Last Modified:		5 Page: Matrix:	1 Water

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	Method Reference
		*** INORG	ANICS ***			
NITRATE		20.0	mg/l	1010	03/15/96	SW 9056
SULFATE		0,2	mg/l	68.3	03/14/96	SW 9056
		*** MEI	ALS ***			
CHROMIUM		5.0	ug/l	ND	03/19/96	SW 6010
LEAD		2.0	ug/l	23.4	03/21/96	SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

- A = NOT APPLICABLE
- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

### SOUTHWEST LABORATORY OF OKLAHOMA, INC.

1700 W. ALBANY SUITE C BROKEN ARROW, OK 74012-1421 (918) 251-2858

Client Name	: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		OCK	
Client ID:	MW - 8 - F	Project ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.30	Report:	24931.30	
Collected: Received:		Report Date: 03/27/19 Last Modified:	96 Page: Matrix:	l Water

TBST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	Method Reference
		*** MET.	ALS ***			
CHROMIUM LEAD		5,0 2.0	ug/l ug/l	ND 23.8	03/19/96 03/21/96	SW 6010 SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

= UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE

Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #EPA600/4-79-020, MARCH 1985

- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCH	2	
Client ID:	MW - 9	Pro	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24948.07	Rep	port:	24948.07	
Collected: Received:	03/14/1996 03/15/1996	Report Date: Last Modified:	03/27/1996	Page: Matrix:	1 Water

TEST	DATE BXTRACTED	DETECTION LIMIT	UNITS	RESULTS	date Analyzed	METHOD REFERENCE
		*** INORG	ANICS ***			
NITRATE		0.2	mg/l	37.3	03/15/96	SW 9056
SULFATE		2.0	mg/l	621	03/19/96	SW 9056
		*** MBT.	ALS ***			
CHROMIUM		5.0	ug/l	ND	03/26/96	SW 6010
LEAD		2.0	ug/l	4.0	03/21/96	SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
  - = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = EPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	E: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROC	ĸ	
Client ID:	MW-9	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24948.08 MS	Re	port:	24948.08	
Collected: Received:		Report Date: Last Modified:	03/27/199	6 Page: Matrix:	1 Water

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE	METHOD REFERENCE
		*** INORG	ANICS ***			
NITRATE		0.2	mg/l	52.7	03/15/96	SW 9056
SULFATE		2.0	mg/l	813	03/19/96	SW 9056
		*** MBT.	ALS ***			
CHROMIUM		5.0	ug/l	172	03/26/96	SW 6010
LEAD		2.0	ug/l	17.5	03/21/96	SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
  - = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT

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- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = EPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	: WOODWARD CLYI 900 SOUTH SI SUITE 412 LITTLE ROCK,		TTLE ROCK		
Client ID:	MW - 9	Proj	ect ID: EI	DORADO	CHEMICAL
SWLO ID:	24948.09 MSD	Repo	ort: 24	1948.09	
Collected: Received:		Report Date: 0 Last Modified:	3/27/1996	Page: Matrix:	1 Water

<u>TEST</u>	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	date Analyzed	METHOD REFERENCE
		*** INORG	ANICS ***			
NITRATE		0.2	mg/l	55.3	03/15/96	SW 9056
SULFATE		2.0	mg/l	807	03/19/96	SW 9056
		*** MET	ALS ***			
CHROMIUM		5.0	ug/l	173	03/26/96	SW 6010
LEAD		2.0	ug/l	19.1	03/21/96	SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
- : UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE

Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985

- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = BPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	2: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCI	K	
Client ID:	MW - 9 - F	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24948.17	Re	port:	24948.17	
Collected: Received:		Report Date: Last Modified:	03/27/1996	5 Page: Matrix:	1 Water

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	Method Reference
		*** MBI	ALS ***			
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	ND ND	03/26/96 03/21/96	SW 6010 SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

= UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = BPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	e: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROC	ĸ	
Client ID:	MW - 9 - F	Pro	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24948.18 MS	Rej	port:	24948.18	
Collected: Received:		Report Date: Last Modified:	03/27/199	6 Page: Matrix:	1 Water

	DATE	DETECTION			DATE	METHOD
TEST	EXTRACTED	LIMIT	UNITS	RESULTS	ANALYZED	REFERENCE
		*** MBT	ALS ***			
CHROMIUM		5.0	ug/l	177	03/26/96	SW 6010
LEAD		2.0	ug/l	18.0	03/21/96	SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

IL

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
- : = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

IA = NOT APPLICABLE

Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #BPA600/4-79-020, MARCH 1985

- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCK		
Client ID:	MW - 9 - F	Pro	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24948.19 MSD	Rej	port:	24948.19	
Collected: Received:		Report Date: Last Modified:	03/27/1996	Page: Matrix:	1 Water

	date Extracted	DETECTION	UNITS	RESULTS	DATE ANALYZED	METHOD REFERENCE
TBST	BAIRAGIBD		ONLID	RESOLITS	ANALI 230	KAPAKAACA
		*** MET	ALS ***			
CHROMIUM		5.0	ug/l	177	03/26/96	SW 6010
LEAD		2.0	ug/l	19.3	03/21/96	SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985

- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	E: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		ITTLE ROCK		
Client ID:	MW-10	Proj	ject ID: E	L DORADO	CHEMICAL
SWLO ID:	24931.09	Repo	ort: 2	4931.09	
Collected: Received:		Report Date: 0 Last Modified:	3/27/1996	Page: Matrix:	1 Water

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	METHOD REFE <u>R</u> ENCE
		*** INORG	ANICS ***			
NITRATE		2.0	mg/l	257	03/15/96	SW 9056
SULFATE		0.2	mg/l	89.0	03/14/96	SW 9056
		*** MBI	ALS ***			
CHROMIUM		5.0	ug/l	ND	03/19/96	SW 6010
LEAD		2.0	ug/l	5.2	03/21/96	SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

- = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE
- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT

J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name		YDE CONSULTANTS- SHACKLEFORD , AR 72211	LITTLE ROCH	τ	
Client ID:	MW-10-F	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.25	Re	port:	24931.25	
Collected: Received:		Report Date: Last Modified:		Page: Matrix:	1 Water

TEST	date Extracted	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	METHOD REFERENCE	
*** METALS ***							
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	ND 3.9	03/19/96 03/21/96	SW 6010 SW 7421	

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

= UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

Methodology: SM - STANDARD METHODS, 16th EDITION, 1985 BPA = #EPA600/4-79-020, MARCH 1985

- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCH	χ	
Client ID:	MW-11	Pro	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.06	Rej	port:	24931.06	
Collected: Received:		Report Date: Last Modified:	03/27/1996	5 Page: Matrix:	1 Water

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	METHOD REFERENCE	
		*** INORG	ANICS ***				
NITRATE		0.2	mg/l	22.1	03/14/96	SW 9056	
SULPATE		2.0	mg/l	578	03/15/96	SW 9056	•
		*** MBT.	ALS ***				
CHROMIUM		5.0	ug/l	ND	03/19/96	SW 6010	
LEAD		2.0	ug/l	ND	03/21/96	SW 7421	

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
  - = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #EPA600/4-79-020, MARCH 1985
- \* SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	900 SOUTH S SUITE 412	WOODWARD CLYDE CONSULTANTS-LITTLE ROCK 900 SOUTH SHACKLEFORD SUITE 412 LITTLE ROCK, AR 72211						
Client ID:	MW-11	Pro	oject ID:	EL DORADO	CHEMICAL			
SWLO ID:	24931.07 MS	Rej	port:	24931.07				
Collected: Received:		Report Date: Last Modified:		Page: Matrix:	1 Water			

TEST	DATE EXTRACTED	DETECTION	UNITS	RESULTS	DATE ANALYZED	Method Reference
		*** INORG	ANICS ***			
NITRATE		0.2	mg/l	40.5	03/14/96	SW 9056
SULFATE		2.0	mg/l	753	03/15/96	SW 9056
		*** MBT.	ALS ***			
CHROMIUM		5.0	ug/l	168	03/19/96	SW 6010
LEAD		2.0	ug/l	17.1	03/21/96	SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

L

R = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

- UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE

Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985

\* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS

D = SURROGATES DILUTED OUT

J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	e: WOODWARD CLYI 900 SOUTH SI SUITE 412 LITTLE ROCK,	HACKLEFORD	LITTLE ROCK	:	
Client ID:	MW-11	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.08 MSD	Re	port:	24931.08	
Collected: Received:		Report Date: Last Modified:	03/27/1996 03/27/1996	Page: Matrix:	1 Water

	DATE	DETECTION			DATE	METHOD	
TEST	EXTRACTED	LIMIT	UNITS	RESULTS	ANALYZED	REFERENCE	
		*** INORG	ANICS ***				
NITRATE		0.2	mg/l	42.4	03/14/96	SW 9056	
SULFATE		2.0	mg/1	731	03/15/96	SW 9056	
		*** MBT	ALS ***				
CHROMIUM		5.0	ug/l	175	03/19/96	SW 6010	
LEAD		2.0	ug/l	17.1	03/21/96	SW 7421	

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

= UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE

Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #BPA600/4-79-020, MARCH 1985

- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J \* ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

### SOUTHWEST LABORATORY OF OKLAHOMA, INC.

1700 W. ALBANY SUITE C BROKEN ARROW, OK 74012-1421 (918) 251-2858

Client Name	2: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROC	ĸ	
Client ID:	MW-11-F	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.22	Re	port:	24931.22	
Collected: Received:	03/13/1996 03/14/1996	Report Date: Last Modified:		6 Page: Matrix:	1 Water

TEST	date <u>extracted</u>	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	Method Reference
		*** MET	ALS ***			
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	ND ND	03/19/96 03/21/96	SW 6010 SW 7421

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

- A = NOT APPLICABLE
- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = EPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	2: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCH	ζ	
Client ID:	MW-11-F	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.23 MS	Re	port:	24931.23	
Collected: Received:	03/13/1996 03/14/1996	Report Date: Last Modified:		5 Page: Matrix:	1 Water

TBST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	date Analyzed	METHOD REFERENCE	
		*** MB	TALS ***				
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	189 19.5	03/19/96 03/21/96	SW 6010 SW 7421	

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
  - = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #BPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	2: WOODWARD CLY 900 SOUTH SI SUITE 412 LITTLE ROCK,	HACKLEFORD	TS-LITTLE ROC	ĸ	
Client ID:	MW-11-F		Project ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.24 MSD		Report:	24931.24	
Collected: Received:	03/13/1996 03/14/1996	Report Da Last Modifi	te: 03/27/199 .ed:	6 Page: Matrix:	1 Water

TEST	date extracted	DETECTION	UNITS	RESULTS	date Analyzed	Method Reference			
*** Metals ***									
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	193 18.5	03/19/96 03/21/96	SW 6010 SW 7421			

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

- UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE 'A = NOT APPLICABLE

Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #BPA600/4-79-020, MARCH 1985

- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	900 SOUTH SUITE 412	LITTLE ROCK, AR 72211						
Client ID:	MW-12	Project	ID: EL DORADO	CHEMICAL				
SWLO ID:	24931.10	Report:	24931.10					
Collected: Received:	03/13/1996 03/14/1996	Report Date: 03/2 Last Modified:		1 Water				

TBST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	METHOD REFERENCE
		*** INORG	ANICS ***			
NITRATE		0.2	mg/l	ND	03/14/96	SW 9056
SULFATE		0.2	ng/l	9.6	03/14/96	SW 9056
		*** MBT.	ALS ***			
CHROMIUM		5.0	ug/l	ND	03/19/96	SW 6010
LEAD		2.0	ug/l	ND	03/21/96	SW 7421

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
- = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

1 = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 BPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = EPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name		YDE CONSULTANTS-L SHACKLEFORD , AR 72211	ITTLE ROCK		
Client ID:	MW-12-F	Pro	ject ID: I	EL DORADO	CHEMICAL
SWLO ID:	24931.26	Rep	ort: 2	24931.26	
Collected: Received:	03/13/1996 03/14/1996	Report Date: Last Modified:	03/27/1996	Page: Matrix:	1 Water

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	Method Reference			
*** METALS ***									
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	ND ND	03/19/96 03/21/96	SW 6010 SW 7421			

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
- = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE
- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = EPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCI	X	
Client ID:	MW-13	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.05	Re	port:	24931.05	
Collected: Received:	03/13/1996 03/14/1996	Report Date: Last Modified:		5 Page: Matrix:	1 Water

	DATE	DETECTION			DATE	METHOD	
TEST	EXTRACTED	LIMIT	UNITS	RESULTS	ANALYZED	REFERENCE	
		*** INORG	ANICS ***				
NITRATE		0.2	mg/l	0.2	03/14/96	SW 9056	
SULPATE		2.0	mg/l	809	03/15/96	SW 9056	•
		*** MET	ALS ***				
CHROMIUM		5.0	ug/l	ND	03/19/96	SW 6010	
LEAD		2.0	ug/l	ND	03/21/96	SW 7421	

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

: = UNABLE TO QUANTITATE DUE TO MATRIX INTERPERENCE

IA = NOT APPLICABLE

Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985

- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROCK		
Client ID:	MW-13-F	Pr	oject ID: E	L DORADO	CHEMICAL
SWLO ID:	24931.21	Re	port: 2	4931.21	
Collected: Received:		Report Date: Last Modified:	03/27/1996	Page: Matrix:	1 Water

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE	METHOD REFERENCE	
		*** MBT	ALS ***				
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	ND ND	03/19/96 03/21/96	SW 6010 SW 7421	

ND = NOT DETECTED ABOVE QUANTITATION LIMIT

B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE

= UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE A = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION
- SW = BPA METHODOLOGY, "#SW846", THIRD EDITION, NOVEMBER 1986

Client Name	E: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		LITTLE ROC	ĸ	
Client ID:	MW-14	Pr	oject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.02	Re	port:	24931.02	
Collected: Received:		Report Date: Last Modified:		5 Page: Matrix:	1 Water

TEST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	METHOD REFERENCE				
*** INORGANICS ***										
NITRATE Sulfate		0.2	mg/1 mg/1	11.9 139	03/14/96 03/15/96	SW 9056 SW 9056				
	*** METALS ***									
CHROMIUM		5.0	ug/l	ND	03/19/96	SW 6010				
LRAD		2.0	ug/l	ND	03/21/96	SW 7421				

.... = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
  - = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

1 = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

Client Name	E: WOODWARD CLY 900 SOUTH S SUITE 412 LITTLE ROCK,		-LITTLE ROCK		
Client ID:	MW-14-F	P	roject ID:	EL DORADO	CHEMICAL
SWLO ID:	24931.18	R	eport:	24931.18	
Collected: Received:	03/13/1996 03/14/1996	Report Date Last Modified	: 03/27/1996 :	Page: Matrix:	1 Water

TBST	DATE EXTRACTED	DETECTION LIMIT	UNITS	RESULTS	DATE ANALYZED	METHOD REFERENCE				
*** METALS ***										
CHROMIUM LEAD		5.0 2.0	ug/l ug/l	ND ND	03/19/96 03/21/96	SW 6010 SW 7421				

...D = NOT DETECTED ABOVE QUANTITATION LIMIT

- B = ANALYTE DETECTED IN BLANK AS WELL AS SAMPLE
- = UNABLE TO QUANTITATE DUE TO MATRIX INTERFERENCE

A = NOT APPLICABLE

- Methodology: SM = STANDARD METHODS, 16th EDITION, 1985 EPA = #EPA600/4-79-020, MARCH 1985
- \* = SURROGATE RECOVERY OUTSIDE OF QC LIMITS
- D = SURROGATES DILUTED OUT
- J = ESTIMATED VALUE: CONCENTRATION BELOW LIMIT OF QUANTITATION

#### APPENDIX C GEOTECHNICAL TEST REPORTS

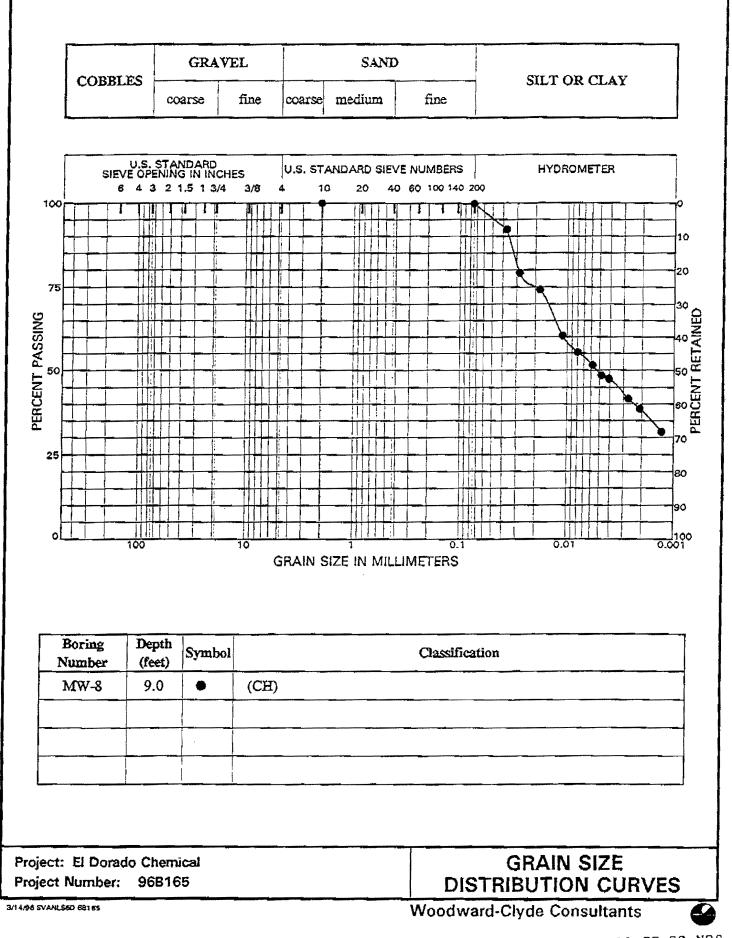
#### Project Name: <u>RI Dorado Chemical</u>

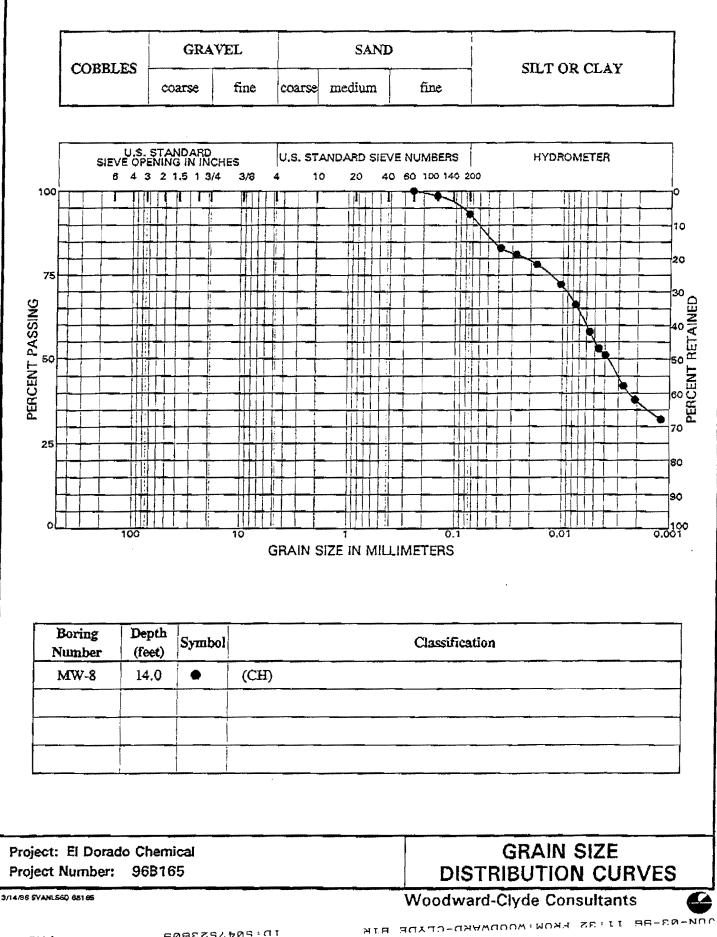
### Project Number: 96B165 Task Number: SIO-2

### SUMMARY OF TEST RESULTS

Subject: In	7 7		Location							· · ·			1					Sheet No.	$\overline{\uparrow}$	
Test			Coordinates WCC			In-Place Density Tests								- #200	Avg. Oven	Perm.	5			
Test tä Number 🕺	Coord	Coordinates			Coordinates			Dry	Water		Proctor O		%	%	LL	PI.	PI	Sieve	Water Content	(cm/sec)
		North	East	No.	Lift	Dry Density (pcf)	Water Content (%)	Curve	d.d. (pcf)	m.e. (%)	Comp. Apprx.	Satur.				(%)	(%) As Rcc.	К <sub>20*С</sub>		
MW-8				1	9'-11'									(CH)						
				<u> </u>	> -11		28.5									93,3*	28.5		_	
MW-8		·		2	14'-16	95.0	26.4					[		(CH)						
										<b>_</b>		ļ	67	26	41	99.8*	26.4			
		 						[]												
una	-	<u> </u>					ļ	<b> </b> ]					<b> </b>						_	
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Remarks:												-			•••••		• L			

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#### APPENDIX B BORING LOGS

DRILLER:       Anderson Engineering       PAGE:       1 of 1 $Hollow-stem Augered:       Hollow-stem Augered:       S.P.T. (b/ft)       Recovery       Description of Stratum         0 0 0 0 0 0 0 1 1 0 0 0 0 0 1 0 0 0 0 0 0 1 0 0 0 0 0 0 1 0 0 0 0 0 0 1 0 0 0 0 0 0 1 0 $	PROJECT: LOCATION CLIENT:	I: El Dor El Dor	or Well Installa ado, Arkansas ado Chemical ado, Arkansas		BORING: FILE: DATE: GEOLOGIST: APPROVED:	MWEDC-01 95B165 2/14/96 EJF
The field       S.P.T.(b/fi)         0          0          1          2          3          4          5          6          7          8          9          10          11          12       Yellow-red and light gray (5YR; 5/8) SILT; medium dense.         6          7          8          9          10          11          12       Yellow-red and light gray (5YR; 5/8) SILT; medium dense.             9          10          11          12          13          14          15          16          17          18       Very stiff dark gray (10YR, 4/2) CLAY; wet.	DRILLER:			9 5		1 of 1
0       r       Recovery (inch)       Description of Stratum         1       -       -       -       -         3       -       -       -       -         4       -       -       12       Yellow-red and light gray (5YR; 5/8) SILT; medium dense.         5       -       -       -       -       -         6       -       -       -       -       -         7       -       -       -       -       -         8       -       -       -       -       -         9       -       16       Light gray (5YR, 7/1) fine Silty SAND; damp to moist.       (MI         11       -       -       -       -       -       -         12       -       -       -       -       -       -       -         11       -	DEPTH (FEET) SYMBOL	SAMPLE				
0       1         1       -         3       -         4       12         5       -         6       -         7       -         8       -         9       -         16       Light gray (5YR, 7/1) fine Silty SAND; damp to moist.         10       -         11       -         12       -         13       -         14       -         15       -         16       Light gray (10YR, 6/4) and tan Clayey SILT; damp.         18       -         19       -         18       Very stiff dark gray (10YR, 4/2) CLAY; wet.		or	Recovery	Descr	ription of Stratum	
9       16       Light gray (5YR, 7/1) fine Silty SAND; damp to moist.       (ML         11       -       1       (ML         11       -       1       (ML         12       -       1       (ML         13       -       1       (ML         14       18       Light gray (10YR, 6/4) and tan Clayey SILT; damp.         15       -       18         16       -       18         17       -       18         18       Very stiff dark gray (10YR, 4/2) CLAY; wet.	1 - 2 - 3 - 4 - - 5 - 6 - 7 -			Yellow-red and light gray (5YR; 5/8) S	ILT; medium dense.	(ML
14       18       Light gray (10YR, 6/4) and tan Clayey SILT; damp.         15       16         16       18         17       18         18       18         19       18         18       Very stiff dark gray (10YR, 4/2) CLAY; wet.	9		16	Light gray (5YR, 7/1) fine Silty SAND	; damp to moist.	(ML/SM
16 - 17 - 18 18 - 19 - 18 Very stiff dark gray (10YR, 4/2) CLAY; wet.	14		18	Light gray (10YR, 6/4) and tan Clayey	SILT; damp.	(ML
10 Very sull dark gray (101R, 4/2) CLAT, wet.	16 - 17 - 18 -					
	20		18	Very stiff dark gray (10YR, 4/2) CLAY End of Boring at 20 <sup>°</sup> .	ζ; wet.	(CL

			LOG	OF BORING				<u></u>
PROJECT: LOCATION:	Monitor Well Insta El Dorado, Arkansa					BORING: FILE: DATE:	MWEDC-02 95B165 2/14/96	
CLIENT: DRILLER:	El Dorado Chemica El Dorado, Arkansa Anderson Engineer	as	ny			EJF LQ 1 of 1		
	Hollow-stem Augered:					PAGE:		
DEPTH (FEET) SYMBOL	SAMPLE							
0-44	S.P.T.(b/ft) or Recover P.Pen.(tsf) (inch)	у		Descr	ription of Stra	tum		
1	]	18 Gray	to dark gray (7.5	YR, 7/2) mediun	n dense Silty	CLAY; damp.		CL
8 - 9 - 10 - 11 -		18 Stiff 1	reddish, yellow ar	nd gray (7.5YR,	7/8) CLAY;	dry.	(1	CL
12 - 13 - 14 - 15 - 16 -	1	18 —stif	f gray (7.5YR, 6/	0) CLAY; wet.				
10-17-		End o	of Boring at 17'.					
							、	
JN 4 96 ENV4B	T2B 5B165 MWEDC-02	<b>6</b> M	Voodward-	Clyde Con	sultants			

			LOG OF BORING			
PROJECT: LOCATION	Monitor V El Dorado	Well Installat o, Arkansas	ion	BORING: FILE: DATE:	MWEDC-03 95B165 2/15/96	
CLIENT:	El Dorado	) Chemical ( ), Arkansas		GEOLOGIST: APPROVED: PAGE:	EIF LO 1 of 1	
DRILLER:		Engineering		PAGE:		
DEPTH (FEET) SYMBOL	Annual Samuel Samue Samuel Samuel S	m Augered:	-			
- 0-144	S.P.T.(b/ft) or P.Pen.(tsf)	Recovery (inch)	Description of Stra	atum		
- 1 - 2 - 3 - 4 - 5 - 6 - 7 - 8 - 9		18	Light gray (5YR, 7/1) Clayey SILT; damp.		(	ML)
- 10-		18	Dense gray (5YR, 6/1) Silty CLAY; traces of reddis	sh brown clay.	(	(CL)
- 11 - - 12 - - 13 -						
- 14 - 15 - 15 - 16 - 17 - 17 - 18 - 19 - 19 - 19 - 19 - 19 - 19 - 19		18	Stiff dark reddish-brown (5YR, 3/2) CLAY.	· .	(	CL)
20- - 21 - - 22 - - 23 -		18	stiff dark gray (5YR, 4/1) CLAY; wet.		(	CL)
- 24-			End of Boring at 24 <sup>r</sup> .			
			·			

CLIENT:	El Dorado El Dorado El Dorado	Chemical C , Arkansas	Company	BORING: FILE: DATE: GEOLOGIST: APPROVED:	MWEDC-04 95B165 2/15/96 EJF ACC				
ORILLER:		n Engineering PAGE: 1 of 1							
(FEET) SYMBOL									
0	S.P.T.(b/ft) or P.Pen.(tsf)	Recovery (inch)	Descriptio	n of Stratum					
		18	Stiff gray (5YR, 6/1) CLAY.		(C)				
8 - 9 - 10 - 11 -		18	stiff gray (5YR, 6/1) CLAY; damp.		(C)				
12 - 13 - 14 - 15 - 16 - 17 - 18 -		18	Gray (5YR, 6/2) stiff CLAY with light gray	plus tan silt lenses; we	t. (CL/M)				
18 - 11 19 - 12 20 - 12			End of Boring at 20 <sup>°</sup> .						



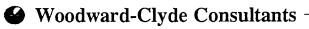
				LOG OF BORING				
PROJ LOCA			Vell Installa ), Arkansas	tion	BOI FIL DA		MWEDC-05 95B165 2/21/96	
CLIE		El Dorado	) Chemical ( ), Arkansas Engineering		GE	OLOGIST: PROVED:	EJF A 1 of 1	
	i		m Augered:	•				
DEPTH (FEET)	SYMBOL	SAMITLE						
- 0-		S.P.T.(b/ft) or P.Pen.(tsf)	Recovery (inch)	Desc	ription of Stratum			
- 1 - 2 - 3 - 4 - 5 - 6 - 7 - 8			18	Moist light gray and tan (5YR, 7/1) Sa	andy CLAY.			(CL)
- 9 - 10-			18	Wet light gray - gray (5YR, $7/1 + 6/1$	) fine SAND and 1	fine Silty SA	AND.	(SM)
- 11 - 12 - 13 - 14								
- 15-				End of Boring at 15'.				
					:			
				_				
				🙆 Woodword-Clyde Cou	ncultonte			]

CLENT:       El Dorado, Arkansas       GEOLOGIST:       El PAGE:         DRILLER:       Anderson Engineering       PAGE:       1 of 1         H       Image:	6
Huge       The form of or or (inch)       Recovery (inch)       Description of Stratum         -       1       -       1       -         -       2       -       1       -         -       3       -       18       Light gray (5YR, 7/1) Clayey SILT; damp; dense.         -       5       -       18       Reddish gray (5YR, 5/2) Silty CLAY; dry to damp.         -       10       18       Reddish gray (5YR, 5/2) Silty CLAY; dry to damp.         -       11       -       18       Wet reddish gray (5YR, 5/2) SILT and Silty SAND.         -       18       -       18       Wet reddish gray (5YR, 5/2) SILT and Silty SAND.	
or         Recovery (inch)         Description of Stratum           1         -	
1       -       1         2       -       18       Light gray (5YR, 7/1) Clayey SILT; damp; dense.         -       -       -       -         -       -       -       -         -       -       -       -         -       -       -       -         -       -       -       -         -       -       -       -         -       -       -       -         -       18       Reddish gray (5YR, 5/2) Silty CLAY; dry to damp.         -       11       -       -         -       12       -       -         -       13       -       -         -       14       -       -         -       18       Wet reddish gray (5YR, 5/2) SILT and Silty SAND.       -         -       -       -       -       -         -       -       -       -       -         -       -       -       -       -         -       -       -       -       -         -       -       -       -       -         -       -       -       -       -	
9       18       Reddish gray (5YR, 5/2) Silty CLAY; dry to damp.         10       11       12         11       12       13         13       14       18         14       18       Wet reddish gray (5YR, 5/2) SILT and Silty SAND.         15       16         18       18         18       18	(ML)
13       -	(CL
	ML/SM

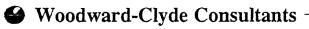


PROJECT: LOCATION: CLIENT: DRILLER:	El Dorado, El Dorado El Dorado,	Chemical C	company	BORING: FILE: DATE: GEOLOGIST: APPROVED: PAGE:	MWEDC-07 95B165 2/20/96 EJF f ( 1 of 1
DEPTH (FEET) SYMBOL	Hollow-sterr				
	S.P.T.(b/ft) or P.Pen.(tsf)	Recovery (inch)	Descript	tion of Stratum	
1 2 3 4 5 6 7		18	Reddish yellow (7.5YR, 6/6) Silty SAND	with traces of light gray S	ILT; dry. (SM
8 - • • • 9 - • • 10 - • • • 11 - •		18	Stiff reddish gray (5YR, 5/2) CLAY.		(CI
12 - 13 - 14 - 15 - 16 -		18	-very stiff dark gray (10YR, 4/1) CLAY		(CI
17 - 18 - 19 - 20		18	Wet, loose light gray (5YR, 7/1) SILT and	fine Silty SAND.	(ML/SM
22# []+-			End of Boring at 22'.		

PROJECT: LOCATION: CLIENT:	El Dorado	Chemical C		BORING: FILE: DATE: GEOLOGIST: APPROVED:	MWEDC-08 95B165 2/20/96 EJF
ORILLER:		, Arkansas Engineering		PAGE:	1 of 1
(FEET) SYMBOL	Hollow-sten	n Augered:			
0	S.P.T.(b/ft) or P.Pen.(tsf)	Recovery (inch)	Descrij	ption of Stratum	
1 - 2 - 3 - 4 - 5 - 6 - 7 - 8 -		18	Fill material consisting of dark brown (5 CLAY, yellow brown medium SAND, a	YR, 7/1 + 10YR, 6/3) Sar and light gray Silty SAND,	dy (SC/S) loose.
9 10		18	Light gray (5YR, 7/1) Silty CLAY; med	ium dense; damp.	(CH
11 12 13 14 15 16 17 18 18		18	Very stiff dark grayish brown (10YR, 4/	1) CLAY.	
19 - 20 - 21 - 22 -		4	Light gray (5YR, 7/1) CLAY and light b	rown fine SAND.	(CL/SN
23 - 24 - 25 - 26 -			wet, light gray (5YR, 7/1) fine Silty S.	AND.	(SM
27			End of Boring at 27'.		

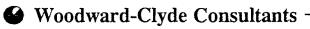


	l Installat Arkansas	FILE: 95B16 DATE: 2/15/9	6
El Dorado, A Anderson En	rkansas gineering	APPROVED: APPROVED:	
Hollow-stem A	ugered:		
S.P.T.(b/ft) or P.Pen.(tsf)	lecovery (inch)	Description of Stratum	
	18	White - light gray (5YR, 8/1-7/1) dense Silty CLAY; dry.	(CI
	18	Light gray (5YR, 7/1) stiff CLAY; damp; with lenses.	(CL/MI
	18	stiff gray (5YR, 7/1) CLAY; moist	(CI
	18	dark gray (5YR, 7/1) stiff CLAY with white to light gray SILT; damp.	(CI
	18	Wet gray (5YR, 7/1) SILT.	(ML
		End of Boring at 28°.	
	El Dorado Ci El Dorado, A Anderson En Hollow-stem A	El Dorado, Arkansas Anderson Engineering Hollow-stem Augered: S.P.T.(b/ft) or P.Pen.(usf) Recovery (inch) 18 18 18 18	El Dorado Chemical Company       DATE:       2715/9         El Dorado Arkanasa       Anderson Engineering       APROVED:       LCR         Anderson Engineering       PAGE:       1 of 1         Hollow-stem Augered:       Image: Company of Stratum       Image: Company of Stratum         S.P.T.(b/ft) of pressure       Recovery (inch)       Description of Stratum         P.P.Pen.(ub)       Recovery (inch)       Description of Stratum         18       White - light gray (5YR, 8/1-7/1) dense Silty CLAY; dry.         18       Light gray (5YR, 7/1) stiff CLAY; damp; with lenses.         18       -stiff gray (5YR, 7/1) CLAY; moist.         18      dark gray (5YR, 7/1) stiff CLAY with white to light gray SILT; damp.



OFCT:	Mor	itor W	Vell Installat	LOG OF BORING -	BORING:	MWEDC-10
			, Arkansas		FILE:	95B165
					DATE:	2/19/96
JENT:			Chemical C	Company	GEOLOGIST:	EJE
			, Arkansas		APPROVED:	1 of 1
ULLER:	And	erson	Engineering		PAGE:	1 01 1
	Ho	low-ster	n Augered:			
(FEET) SYMBOL	SAMPLE					
SYN (FE	SAN					
		T.(b/ft) or	Recovery (inch)	Descri	ption of Stratum	
0-	P.F	en.(tsf)	(inch)		• · · · · · · · · · · · · · · · · · · ·	
1-1/						
2 - 1						
3-1/						
4				SALE		
5-11			16	Stiff gray (5YR, 6/1) CLAY; dry.		(C
6-11	3					
7	1					
. II						
			18	Stiff reddish gray (5YR, 5/2) Silty CLA dry to damp.	Y with traces of yellow Silt	y SAND; (C
				dry to damp.		
	1					
$\frac{2}{2}$						
3 -						
4	1		18	Reddish brown $(5YR, 5/2 + 7/1)$ CLAY and yellow fine sand lenses; wet.	with intermittent light brow	wn SILT (CL/SN
5-				and yellow line sand lenses; wet.		
6 -						
7 -						
8 -						
9 -						
0-404	1			End of Boring at 20'.		
	E I					

			LOG OF BORING		
	El Dorado			BORING: FILE: DATE:	MWEDC-11 95B165 2/19/96 F IF 0
CLIENT:	El Dorado	Chemical C , Arkansas		GEOLOGIST: APPROVED:	EJF LOI 1 of 1
DRILLER:	Anderson Hollow-ster	Engineering		PAGE:	1 01 1
UEPTH (FEET) SYMBOL	SAMPLE				
0	S.P.T.(b/ft) or P.Pen.(tsf)	Recovery (inch)	Descriptio	on of Stratum	
1		18	Loose, damp, light gray (5YR, 7/1) and tan	Silty CLAY.	(C)
9 10 11 12 		18	Stiff red-gray (5YR, 5/2) CLAY; with intergray silt lenses; damp to moist.	mittent tan fine sand and	l light (CL/M)
13 - 14 - 15 - 16 - 17 -		18	Light gray, tan and reddish brown (10YR, 6 with silty sand lenses.	5/6) fine-medium SAND	; wet; (SN
18 – 19 19 – – – – – – – – – – – – – – – – – – –			End of Boring at 19 <sup>7</sup> .		



PROJECT:	Monitor W	Vell Installat	ion	BORING:	MWEDC-12
LOCATION:	El Dorado, Arkansas			FILE:	95B165
<u> </u>		~		DATE:	2/19/96
CLIENT:	El Dorado	Chemical C	Company	GEOLOGIST: APPROVED:	EFR
DRILLER:		, Arkansas Engineering		PAGE:	1 of 1
	,		· · · · · · · · · · · · · · · · · · ·		
(FEET) SYMBOL					
0	S.P.T.(b/ft) or P.Pen.(tsf)	Recovery (inch)	Descrij	ption of Stratum	
1 - 2 - 3 - 4 - 5 - 6 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 8 - 7 - 7		14	Loose, moist gray (10YR, 6/4) CLAY; v sandy clay and traces of small gravel.	with light gray and yellow t	orown (CI
9		18	Wet light gray (5YR, 7/1) and tan Claye	y SILT.	(MI
10					
14 15 16		18	wet gray (5YR, 7/1) Clayey SILT with	n traces of tan fine Silty SA	ND. (ML/SM
17- <b>1</b> 11			End of Boring at 17'.		
	]		-		

			LOG OF BORING —		
ROJECT: OCATION:	El Dorado	Vell Installat , Arkansas		BORING: FILE: DATE:	MWEDC-13 95B165 2/14/96
LIENT: RILLER:	El Dorado	Chemical C , Arkansas Engineering		GEOLOGIST: APPROVED: PAGE:	EJF 1 of 1
	Hollow-ster				
(FEET) SYMBOL					
0	S.P.T.(b/ft) or P.Pen.(tsf)	Recovery (inch)	Descrip	otion of Stratum	
1		18	Medium dense Silty CLAY; light pinkish 6/2 - 6/3).	a gray to light reddish brow	m (5YR, (C
8 - 9 - 10 - 11 - 12 -		. 18	Reddish gray (5YR, 5/2) Clayey SILT w light gray silt.	ith traces of yellow-red fin	e sand and (M
13 - 14 14 - 15 15 - 1 • • • 16 - • • • 17 - • • •		18	Dark gray to dark reddish brown (7.5YR SILT; grading to dark gray fine silty san	, 5/0) dense Silty CLAY a d; wet.	nd Clayey (ML/SN
			End of Boring at 18'.		

			LOG OF BORING		
PROJECT: LOCATION:	Monitor V El Dorado	Vell Installa , Arkansas	tion	BORING: FILE: DATE:	MWEDC-14 95B165 2/13/96
CLIENT: DRILLER:	El Dorado	Chemical ( , Arkansas Engineering		GEOLOGIST: APPROVED: PAGE:	EJF KCC 1 of 1
	Hollow-ster			TAGE.	
DEPTH (FEET) SYMBOL					
0	S.P.T.(b/ft) or P.Pen.(tsf)	Recovery (inch)	Descriptio	on of Stratum	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		17	Fine Silty SAND; light gray and tan in colo	or (7.5YR, 7/0).	(SM)
- 9		18	Silty CLAY with traces of silt and fine sand (7.5YR, 5/0); damp.	l; light to dark gray in co	lor (CL)
- 13 - 14 - - 15 - - 16 -		18	Wet fine SAND, primarily gray with traces 6/0-7/0) fine sand.	of tan and light brown (	7.5YR, (ML)
- 17			End of Boring at 17'.		
-					

[				LOG OF BORING		
PROJE		Monitor V El Dorado	Vell Installat Arkansas	ion	BORING: FILE:	MWEDC-15 95B165
					DATE:	2/13/96
CLIEN	T:		Chemical C , Arkansas	ompany	GEOLOGIST: APPROVED:	Effd
DRILL	ER:		Engineering		PAGE:	1 of 1
		Hollow-ster	n Augered:			
DEPTH (FEET)	SYMBOL					
E E	SΥ	¥6				
		S.P.T.(b/ft)	Pacouaru	Descriptio	an of Strotum	
└ o-		or P.Pen.(tsf)	Recovery (inch)	Descriptio	on of Stratum	
- 1 - - 2 - - 3 - - 4 - - 5 - - 6 - - 7 - - 8 -			18	Fine Silty SAND; damp; gray (7.5YR, 7/0)		
- 9 -	Ħ		18	Light gray to dark gray (7.5YR, 7/0) Clayey silty sand; wet; dense.	y SILT, with traces of li	ght brown (ML)
- 10- - 11-				sitty saint, wet, dense.		
- 12 -						
- 13 - - 14 -			18	Clayey SILT with lenses of coarse sand a dark brown (7.5YR, 7/0).	nd gravel; wet; dense; g	ray with (ML/GM)
- 15-	114		<b>-</b>  -	End of Boring at 15'.		
						-
	[					
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	l	L				
11151 4 07 1		TOD CD126 1 MINT	DC 15	Woodward-Clyde Consul	ltants ———	
JUN 4 96 E	:NV4B	T2B 5B165 MWE	UC-13			

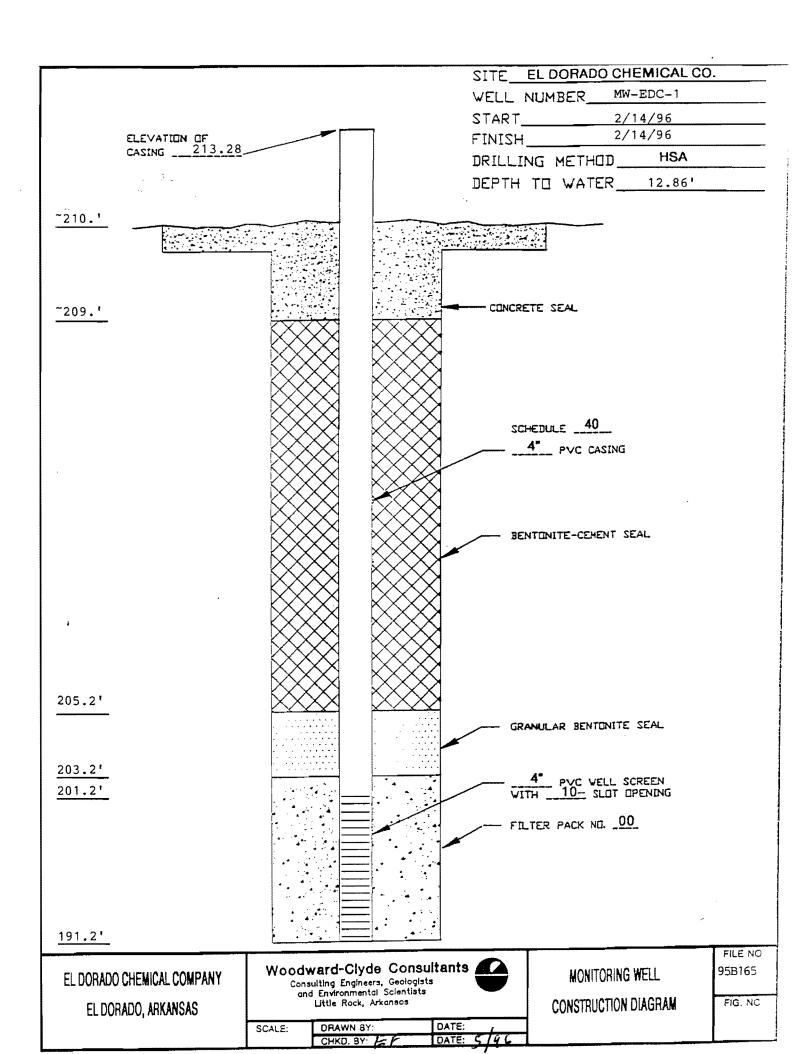
				LOG OF BORING				
PROJE LOCAT			Well Installa lo, Arkansas	tion	BORIN FILE: DATE		MWEDC-16 95B165 2/12/96	
CLIEN	T:		o Chemical o, Arkansas	Сотрапу		OGIST:	E	
DRILL	ER:	Andersor	n Engineerin	3	PAGE:		1 of 1	
DEPTH (FEET)	SYMBOL	SAMPLE	em Augered:					
- 0-		S.P.T.(b/fi or P.Pen.(tsf	Recovery	D	escription of Stratum			
- 1 - 2 3			15	Moist fine SAND and Silty SAND;	tan - white in color (7.5	Y <b>R,</b> 7/7).		(SM)
- 9 -			12	Wet Sandy and Silty CLAY; gray i	n color (7.5YR, 7/0-7/6)			(CL)
- 10- - 11 - - 12 - - 13 -								
- 14 - - 15 - - 16 -			20	Wet fine SAND and SILT, stiff; gr	ay in color (7.5YR, 6/0)			(SM)
- 17	╡┇╡			End of Boring at 17 <sup>+</sup> .				
				-				

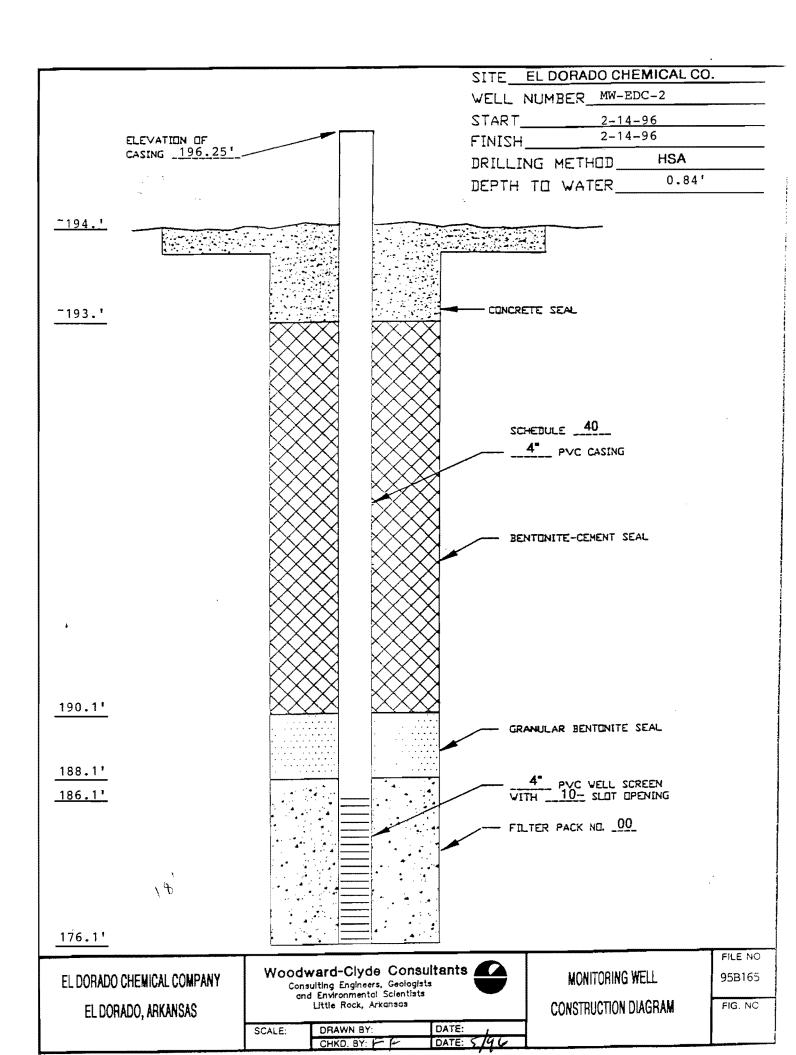


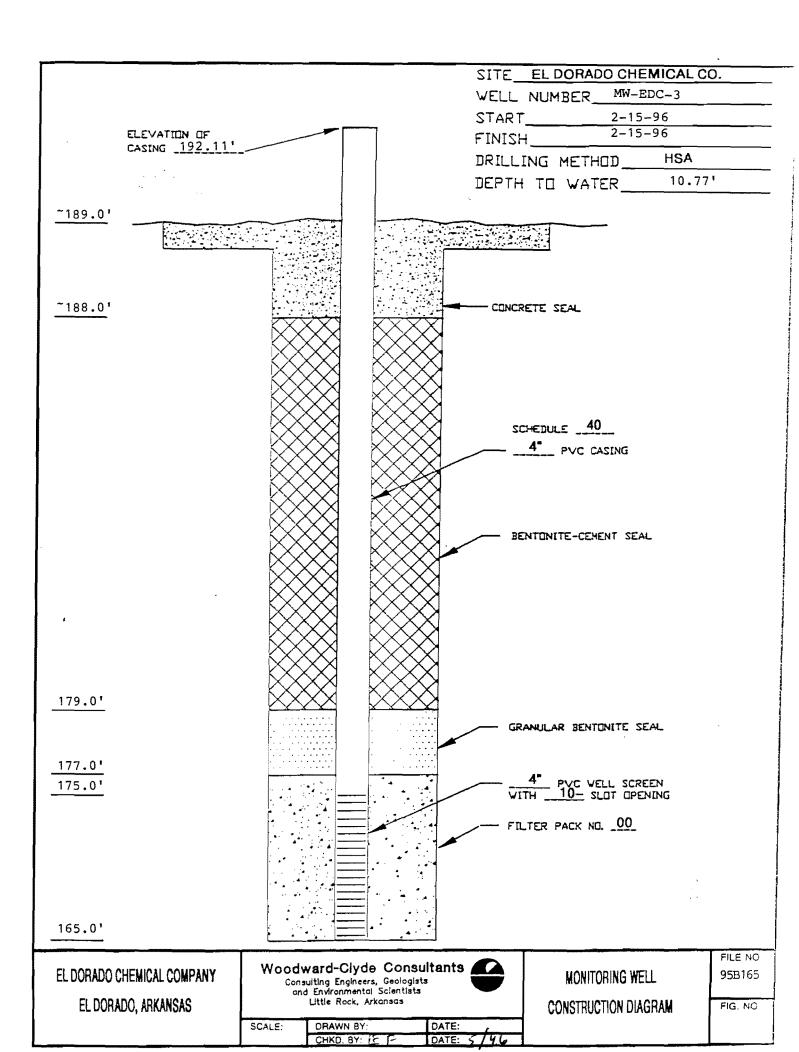
PROJECT: LOCATION: CLIENT: DRILLER:	Monitor W El Dorado, El Dorado El Dorado, Anderson H	Arkansas Chemical C Arkansas	Company	BORING:MWEDC-17FILE:95B165DATE:2/13/96GEOLOGIST:EJFAPPROVED:PAGE:I of 1		
(FEET) SYMBOL	Hollow-stem	a Augered:				
0	S.P.T.(b/ft) or P.Pen.(usf)	Recovery (inch)	Descript	tion of Stratum		
1 2 3 4 5 6 7		2	Red (10YR,4/6) Sandy CLAY.		(S	
8		18	Pinkish gray (5YR, 6/2) fine Silty SAND	with trace of gray clay.	(\$	
14 - 1 15 - 1 16 - 1 17 - 1 18 - 1		12	light gray (5YR, 6/2) fine Silty SAND;	dry; with a trace of tan S	AND.	
19		18	light gray (5YR, 7/1) fine SAND and Si fine sand and dark gray clay.	ilty SAND, with traces of	f yellow	
24 - • • 25 - • • 26 - • • 27 - • • 28 - • •		18	light gray (5YR-7.5YR, 7/0) fine SAND	D; damp.		
29 - 30 - 31 - 32 - 33 -		18	light gray (7.5YR, 7/0) fine SAND and	silt; wet.		
34			End of Boring at 34'.			

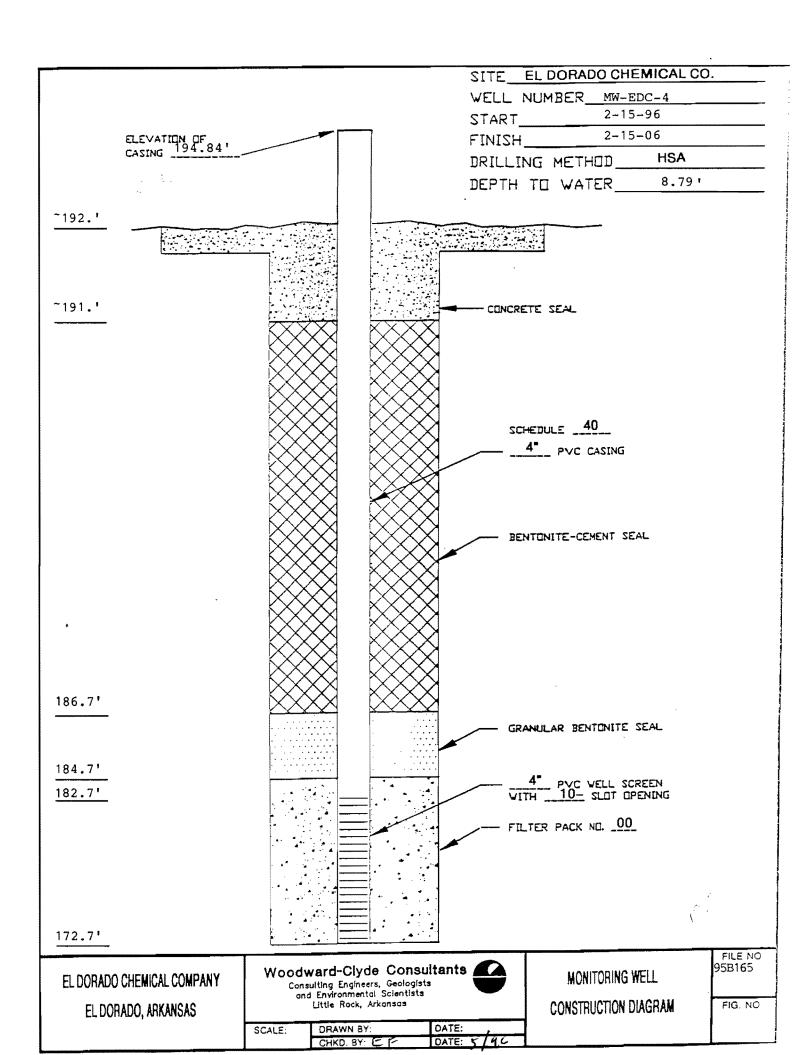
[			LOG OF BORING -			
	El Dorado			BORING: FILE: DATE:	MWEDC-18 95B165 2/22/96	
CLIENT: DRILLER:	El Dorado	Chemical ( , Arkansas Engineering		GEOLOGIST: APPROVED: PAGE:	EJE f of 1	
DEPTH (FEET) SYMBOL	Hollow-ster	m Augered:				
SYI (F						
- 0- <del>11</del>	S.P.T.(b/ft) or P.Pen.(tsf)	Recovery (inch)	Descrip	ption of Stratum		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		18	Damp to wet gray (5YR, 5/1) Clayey SI	LT.	(ML)	
- 9 - 11 - 10		18	Wet light brown-yellow brown (5YR, 7/2 of light gray silty sand.	1) fine to medium SAND w	ith traces (SM)	
- 13 - • • • - 14 - • • •			End of Boring at 14'.			

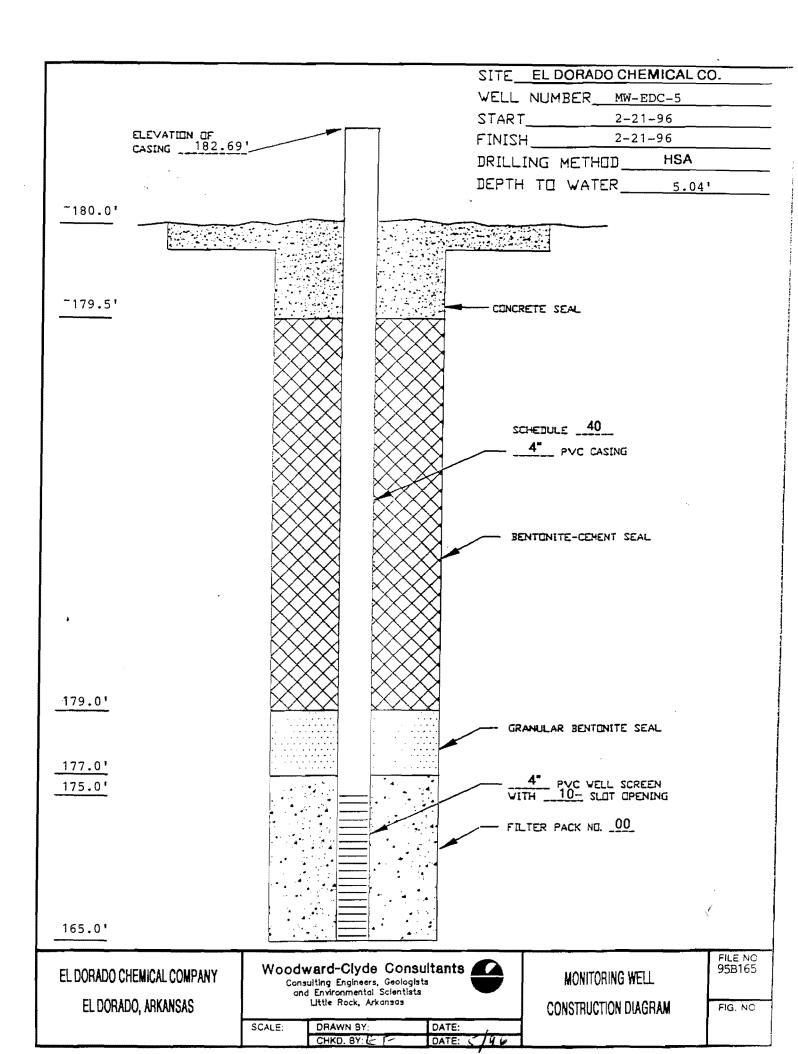
## APPENDIX A MONITORING WELL COMPLETION DIAGRAMS

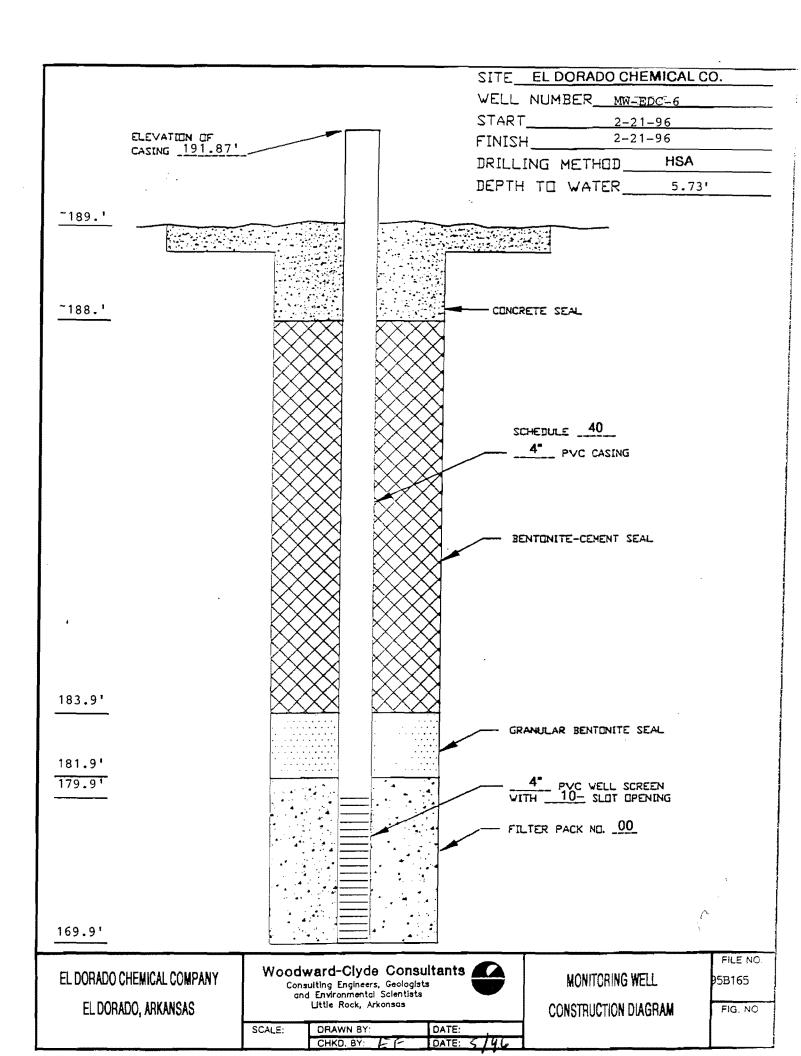


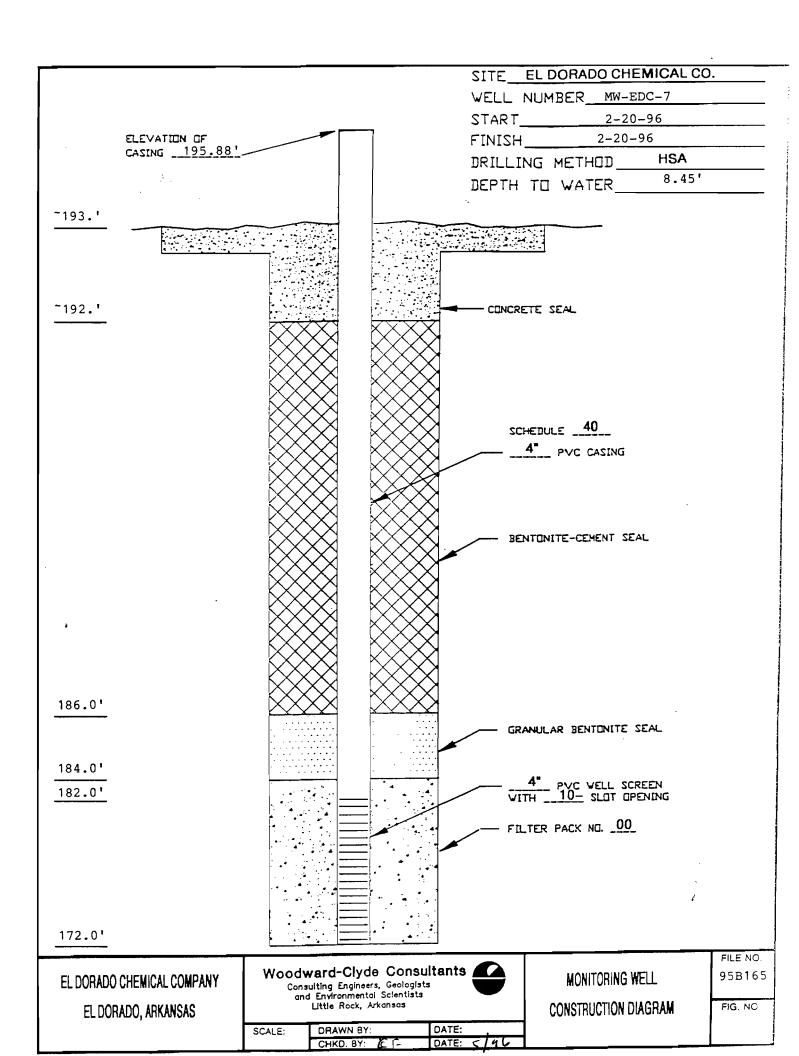


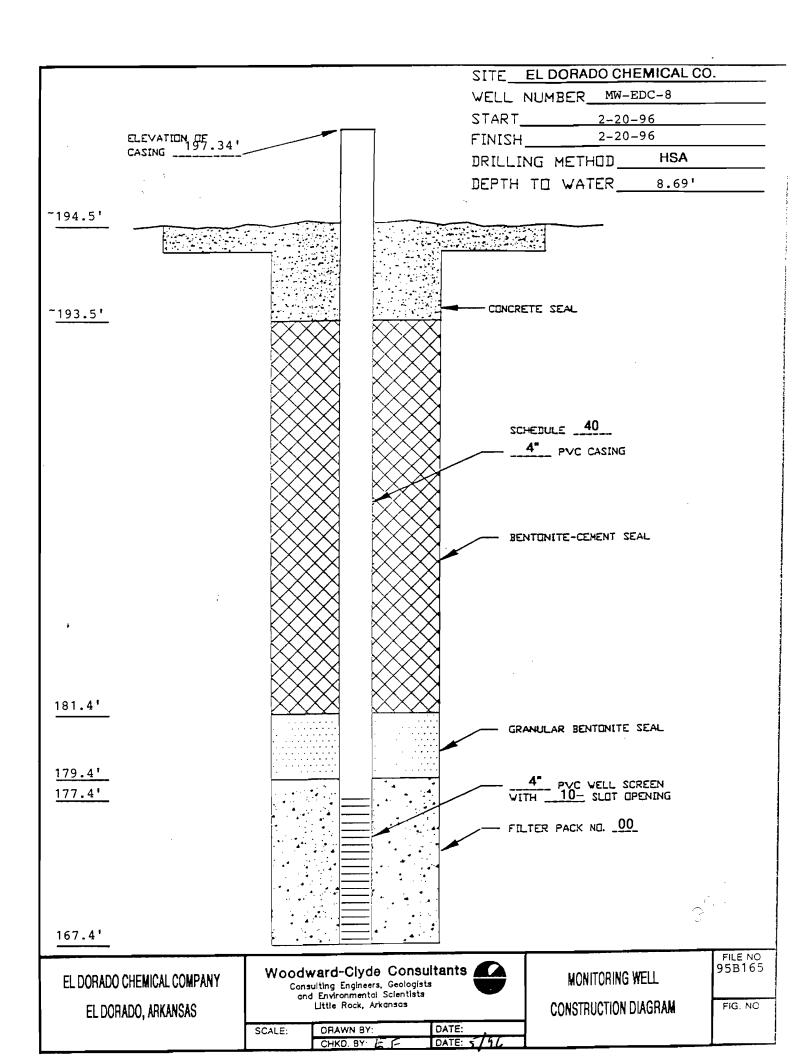


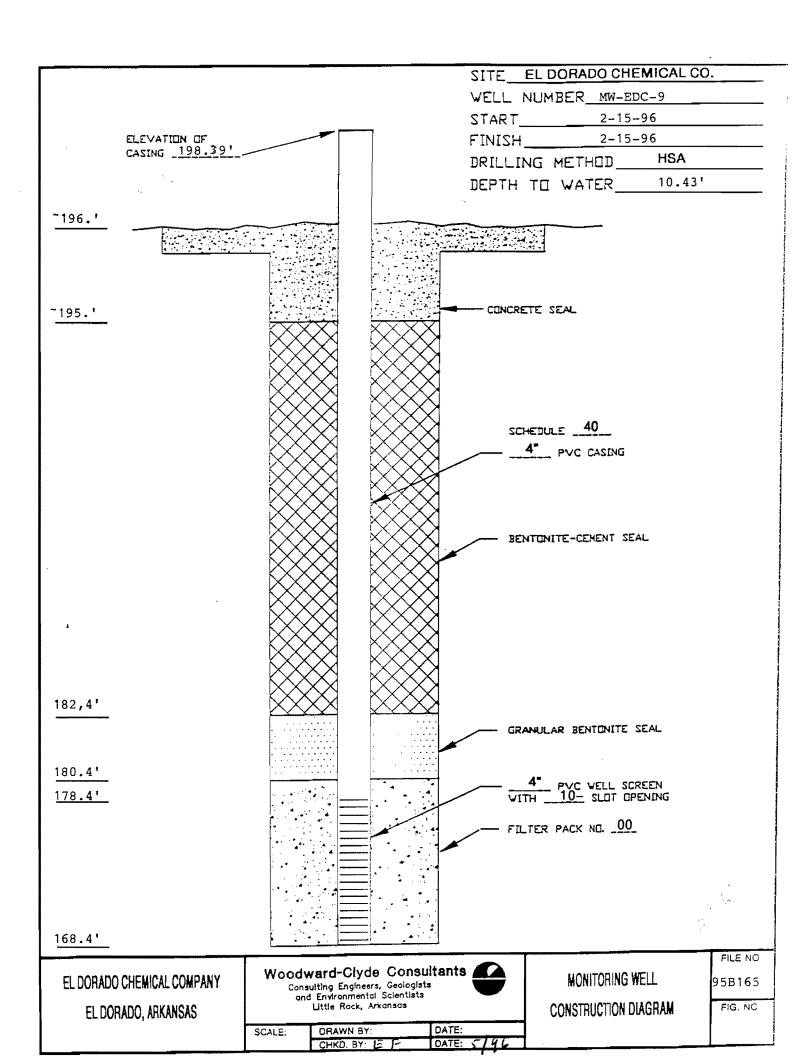


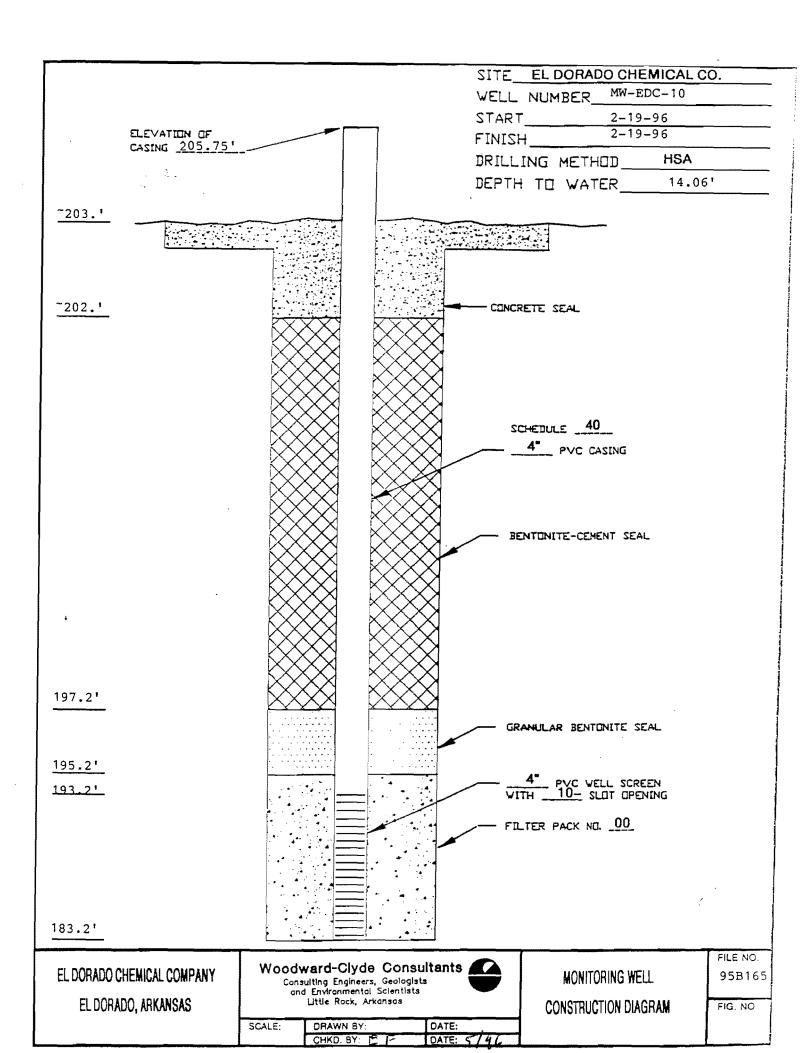


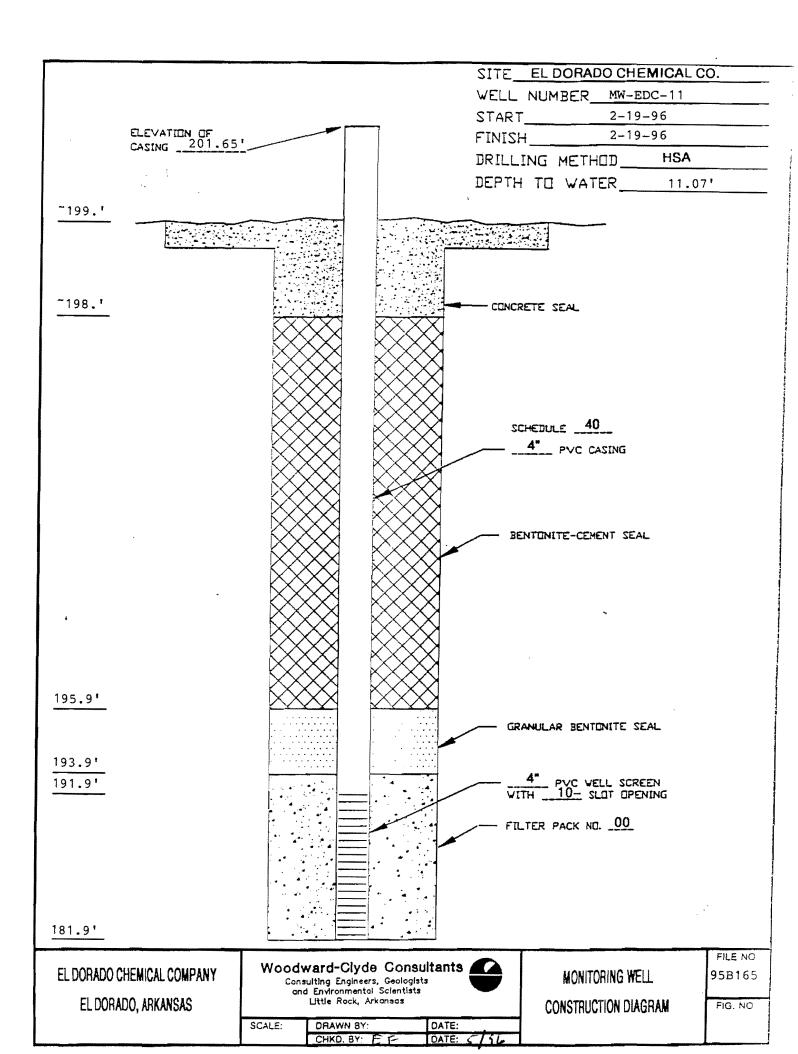


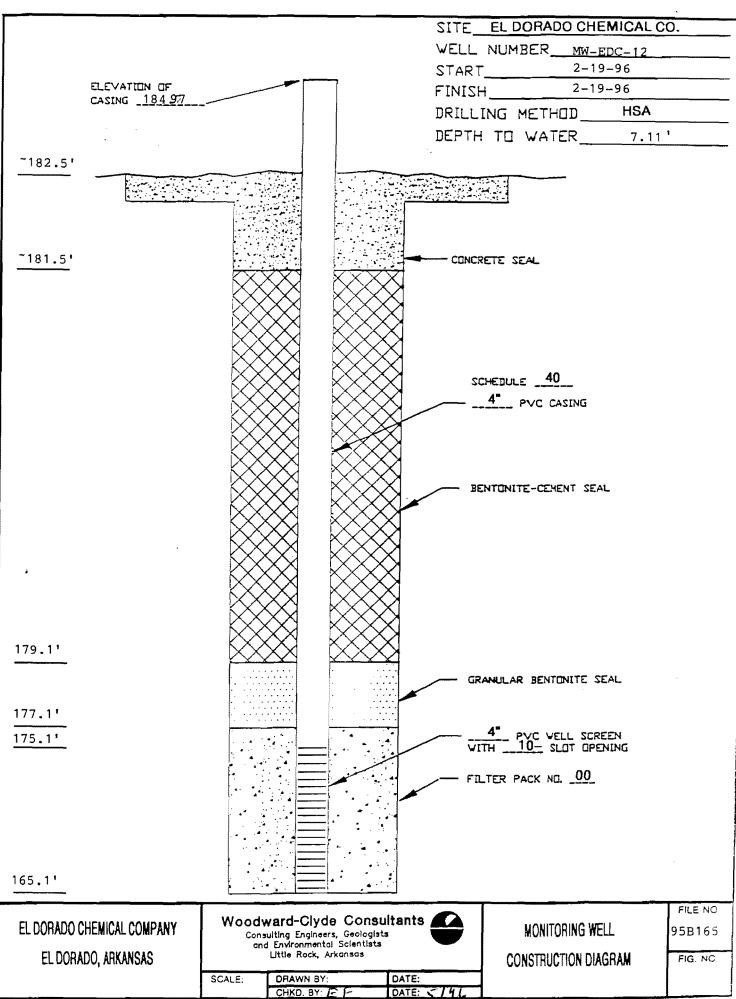


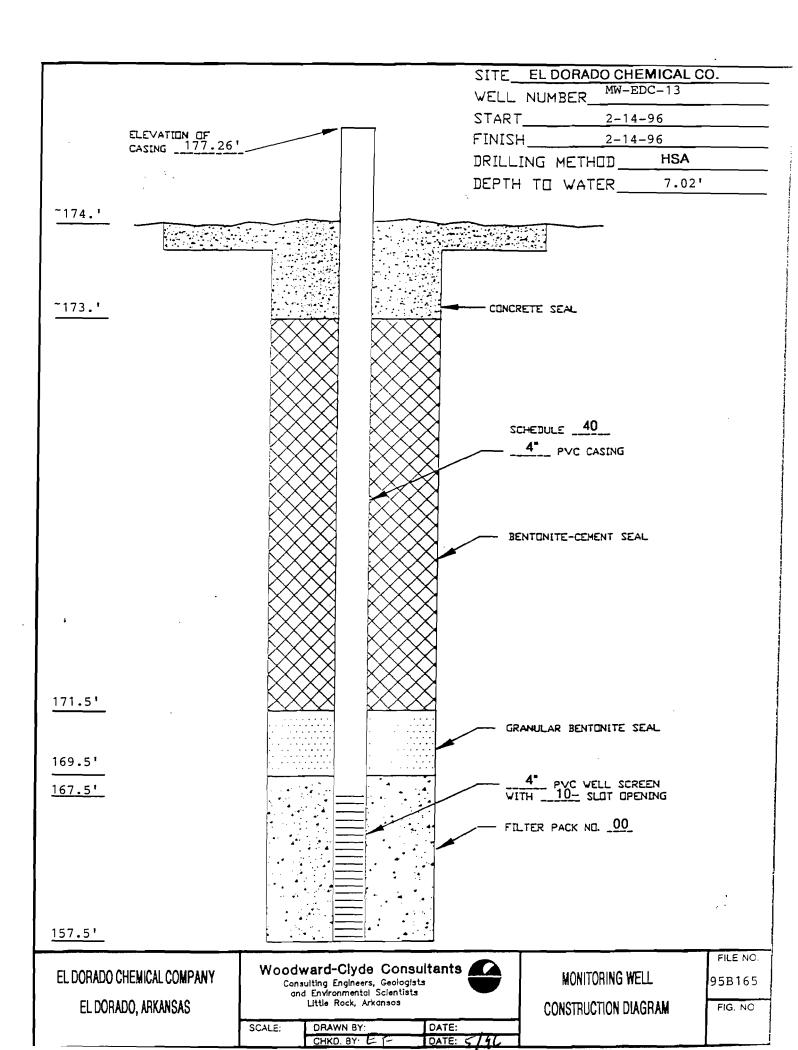


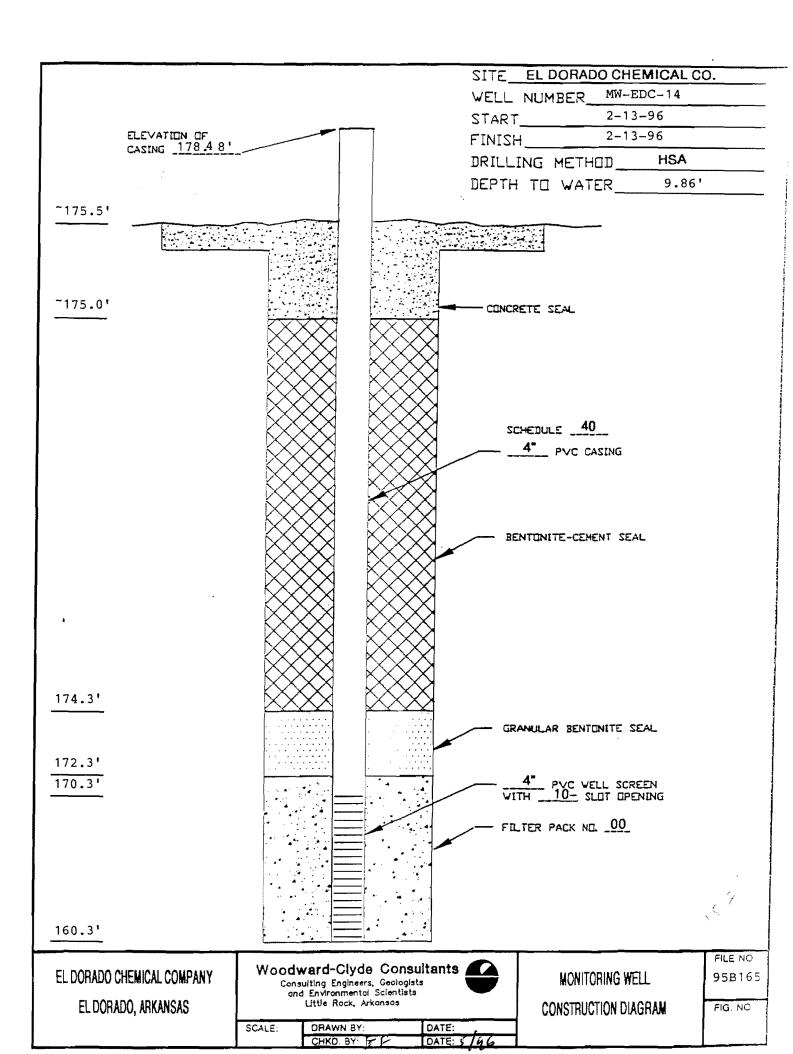


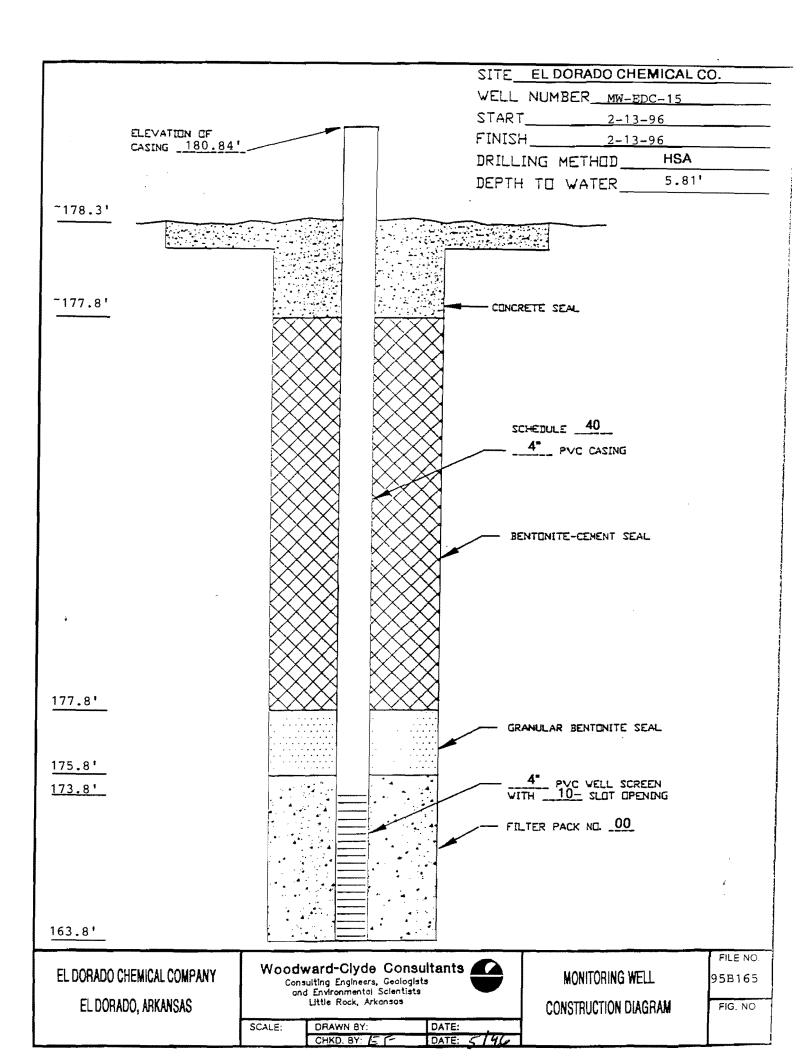


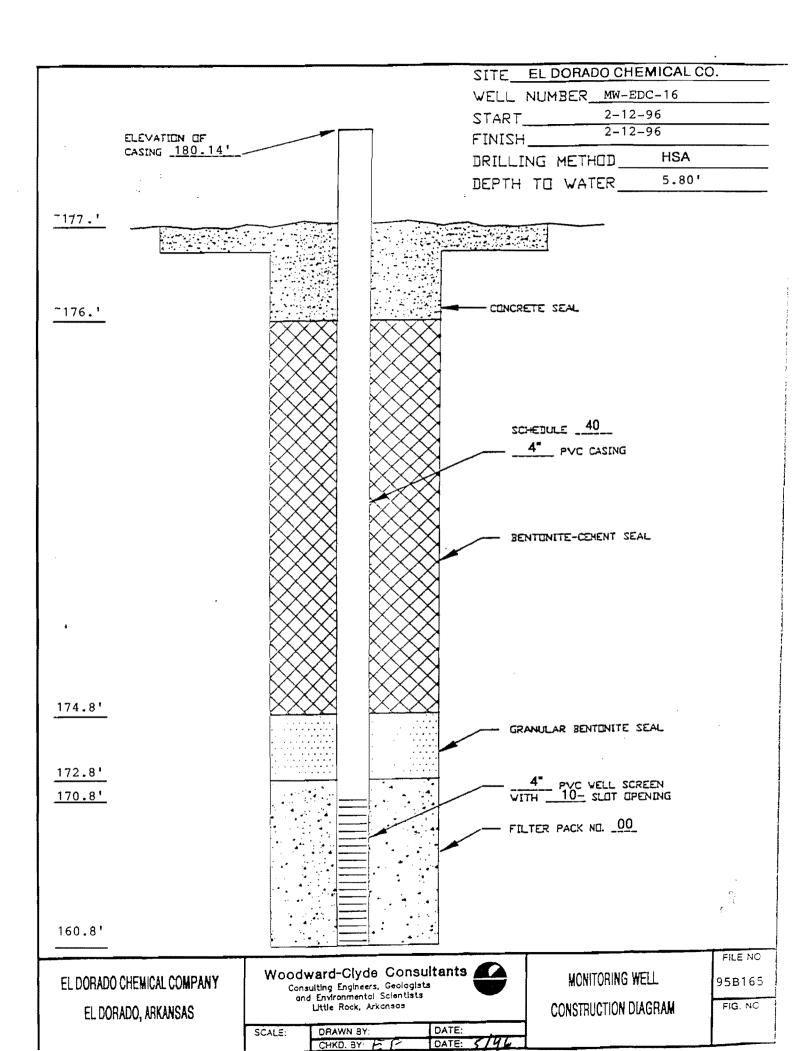


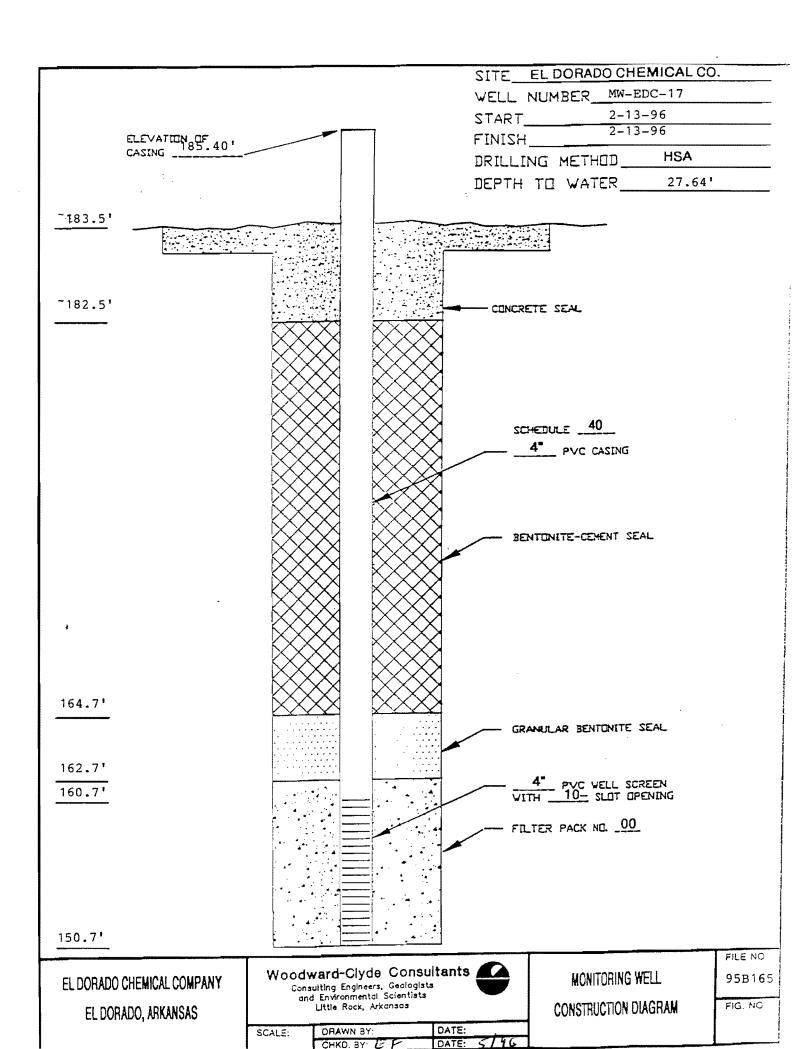


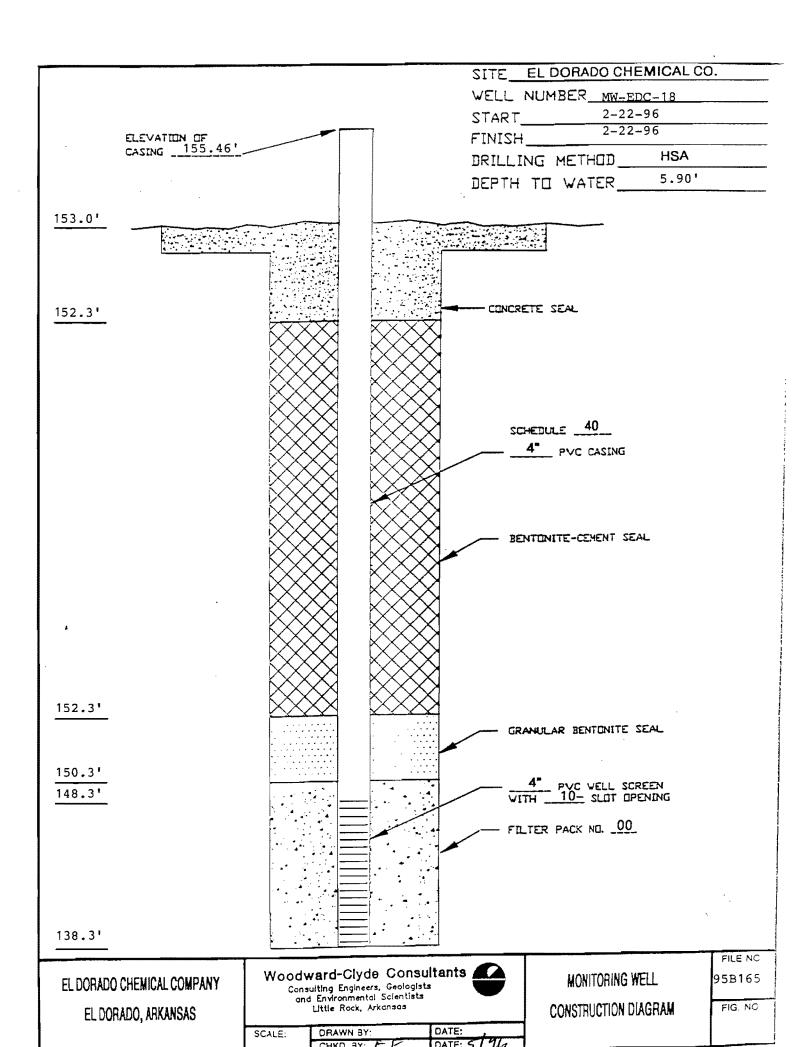


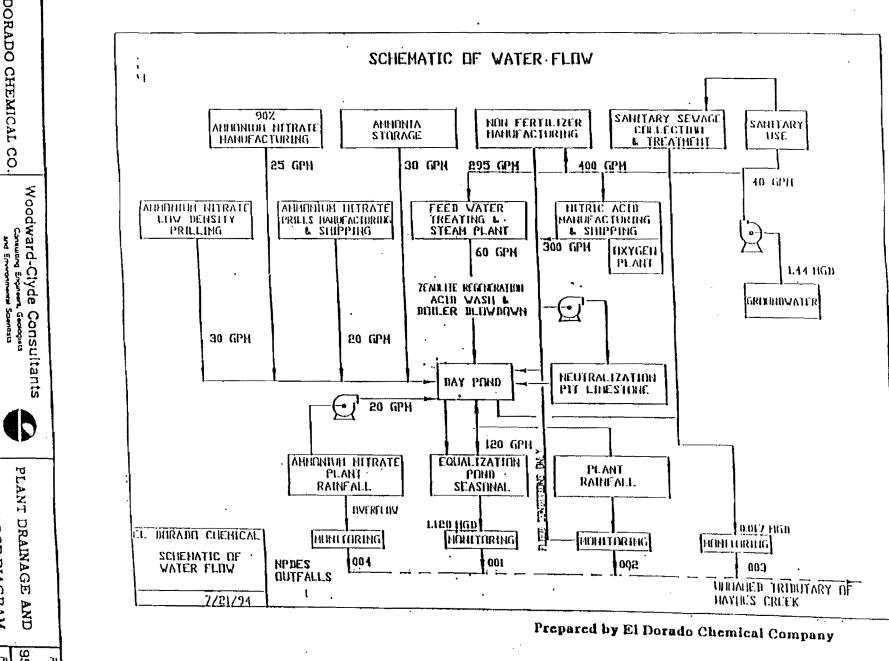












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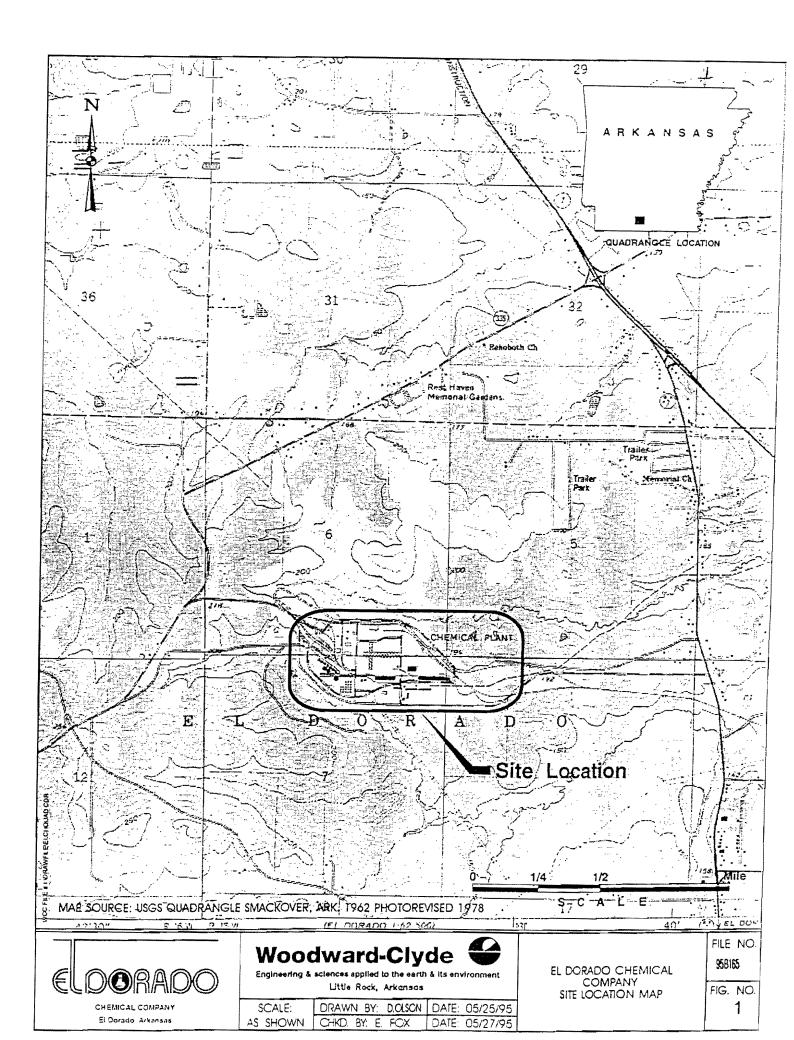
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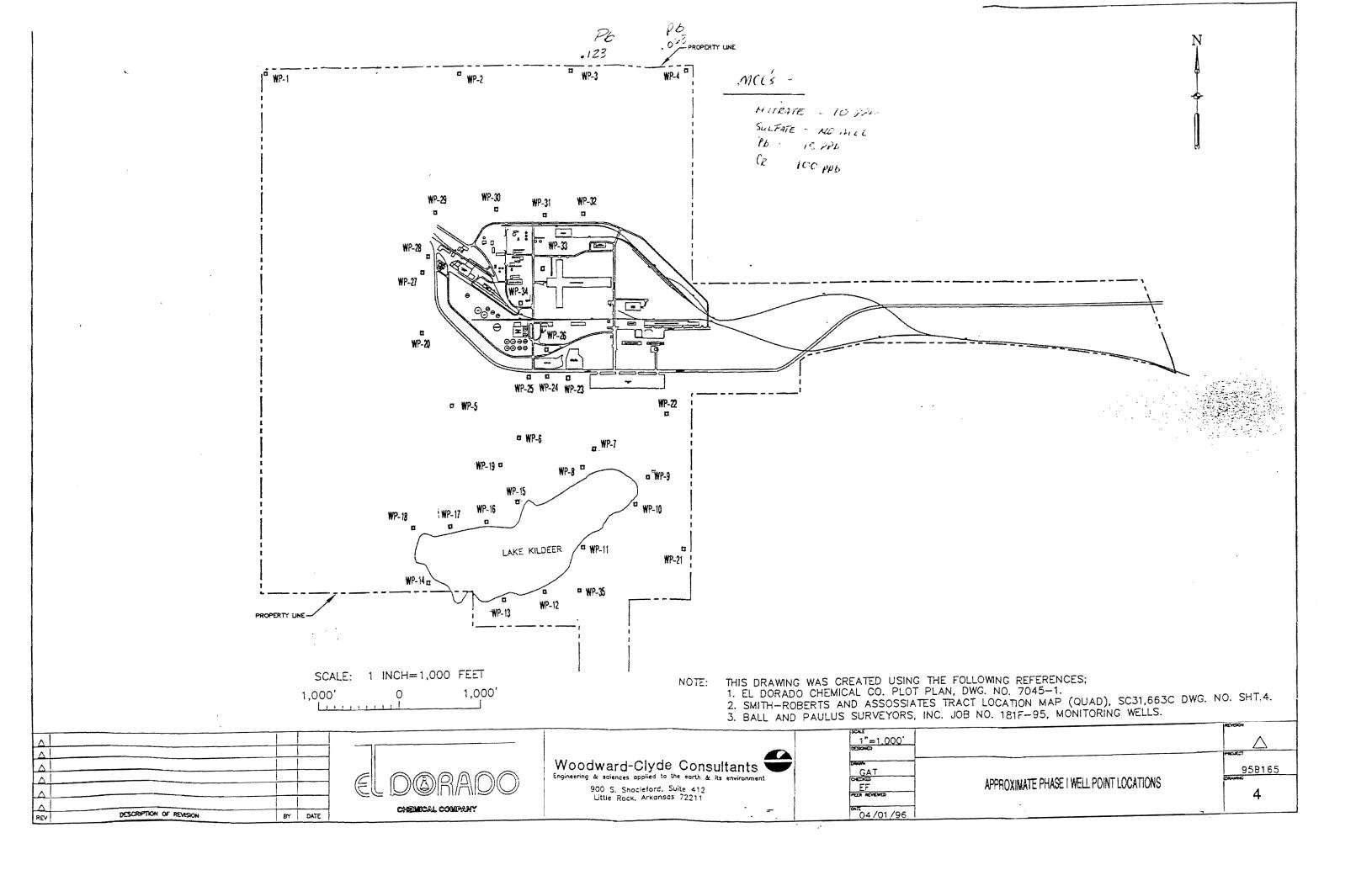
DISCHARGE DIAGRAM

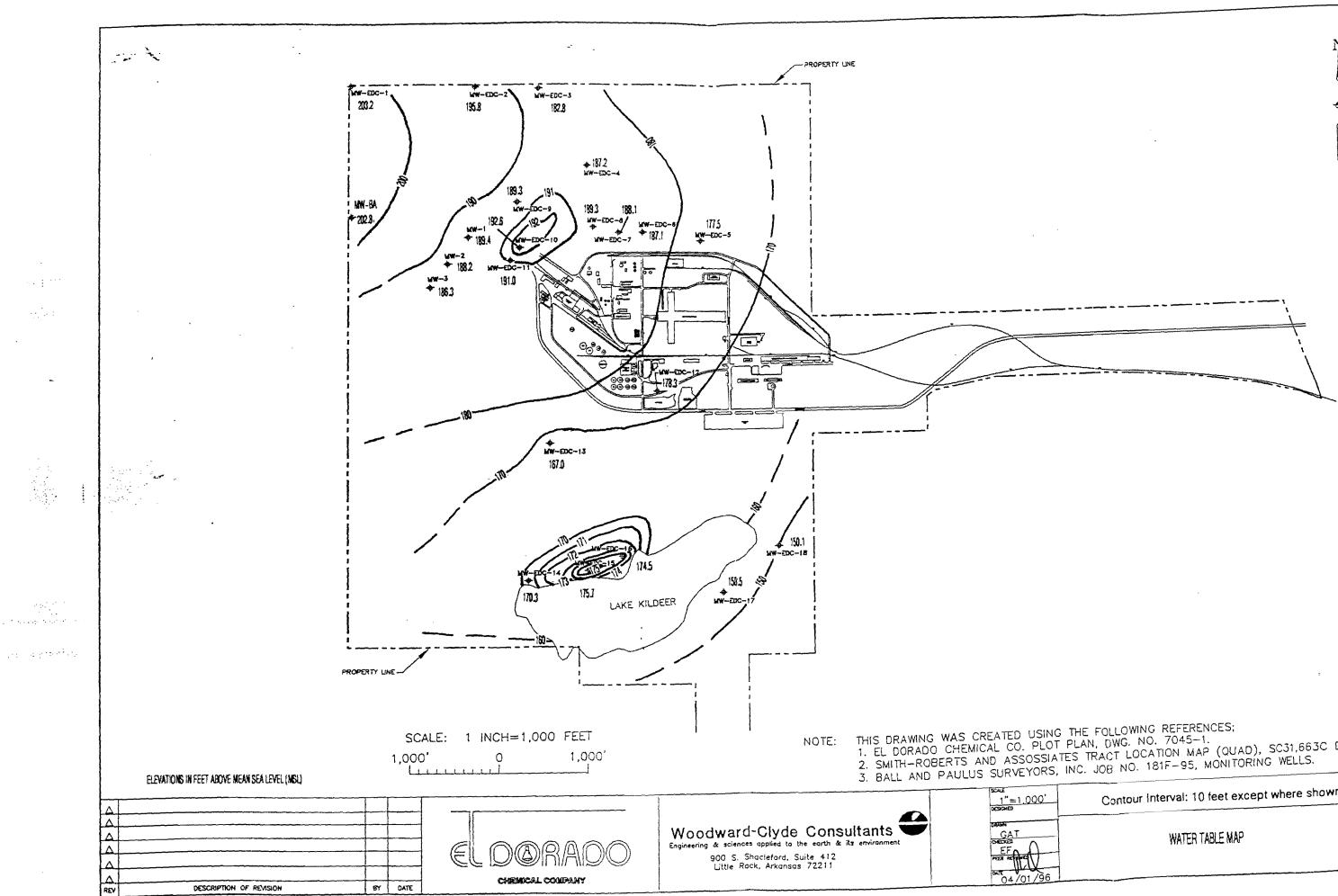
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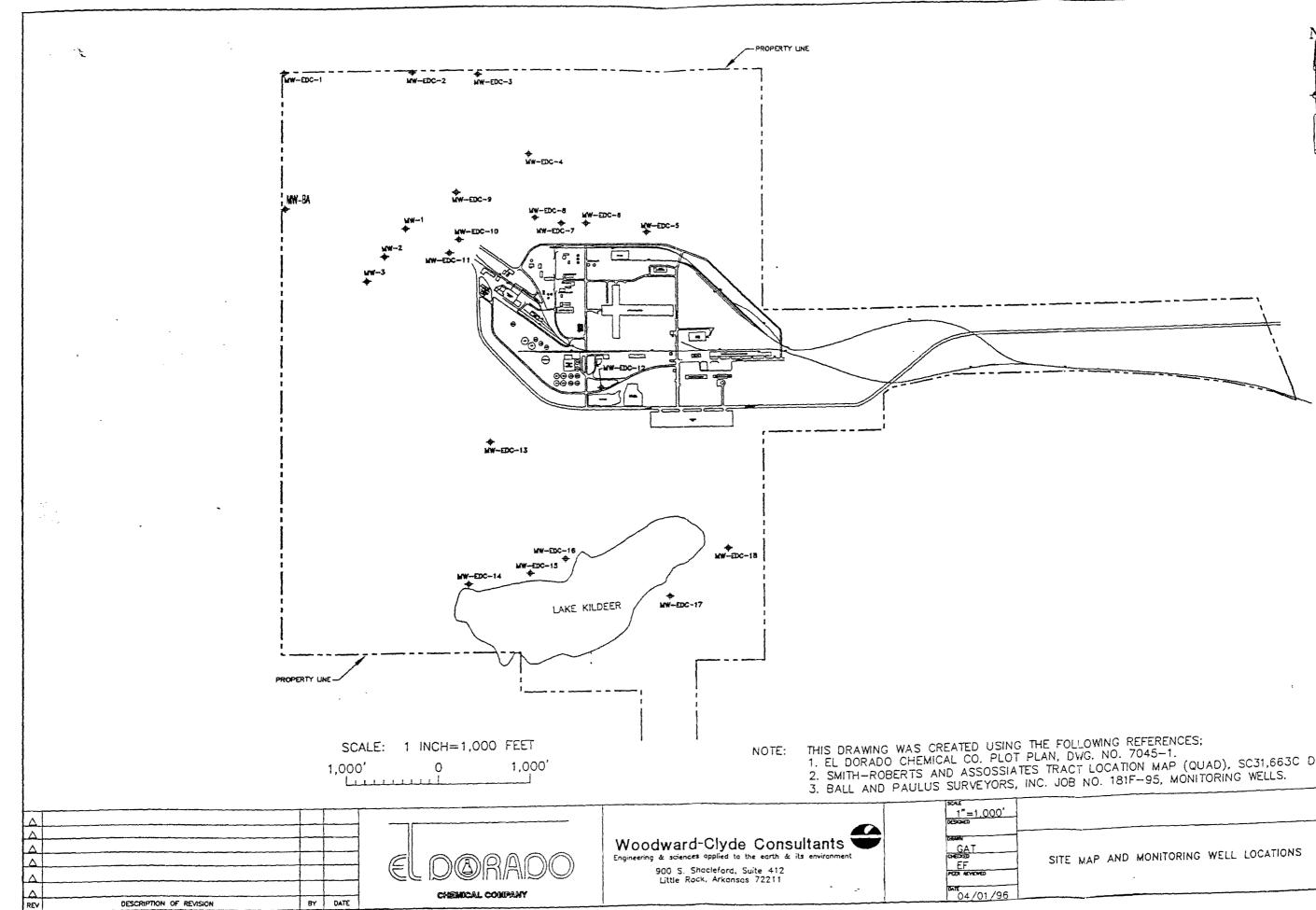
FIGURES







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THE FOLLOWING REFERENCES; PLAN, DWG. NO. 7045-1. IS TRACT LOCATION MAP (QUAD), SC31,663C DWG. NO NC. JOB NO. 181F-95, MONITORING WELLS.	). SHT.4.
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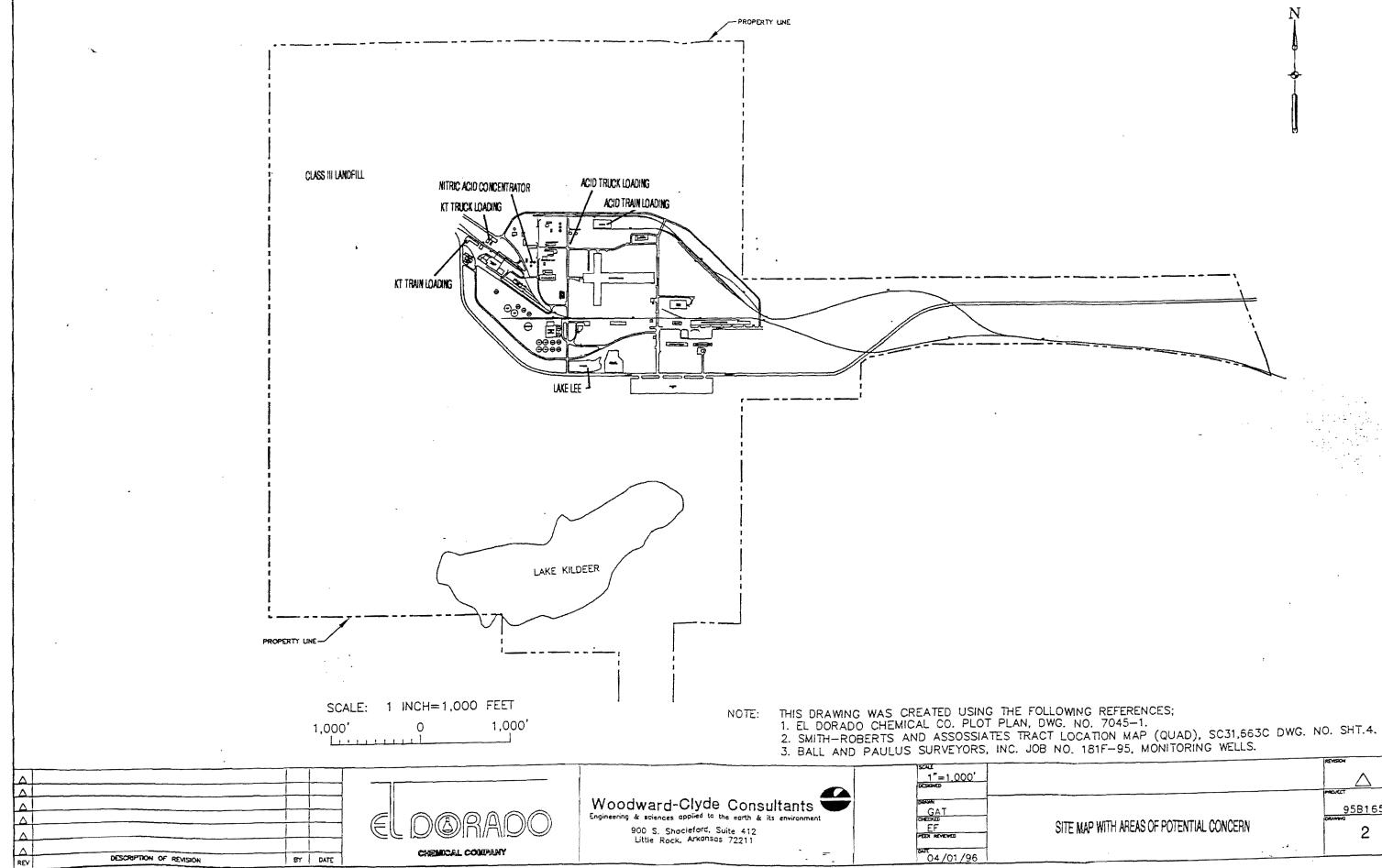
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SITE MAP AND MONITORING WELL LOCATIONS	958165 958765 5



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SITE MAP WITH AREAS OF POTENTIAL CONCERN

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